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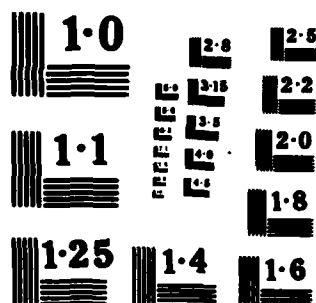
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CONTROL AND SIGNAL CONDITIONING  
CIRCUITS FOR E.I.R.M.A.

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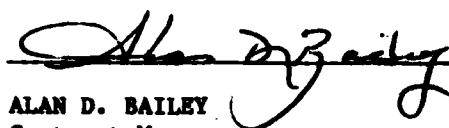
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<p>This report describes the control and the signal conditioning circuits for the Energetic Ion Retarding Mass Analyzer (EIRMA). The control electronics executed commands received from a main control unit of a multi-instrument rocket experiment. The received instructions were converted into the control signals for the ion mass filter. Signal conditioning was provided.</p> <p><i>revised 1/85</i></p>				
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## I. INTRODUCTION

The Energetic Ion Retarding Mass Analyzer (EIRMA) was developed by the Ionospheric Disturbances and Modifications Branch of the Ionospheric Physics Division of the Air Force Geophysics Laboratory for use in the Beam Emission Rocket Test-1 (BERT-1). During the experiment, the potential of a section of a sounding rocket payload was to be modified with respect to the ambient plasma. The vehicle was to be charged positive by the ejection of electrons and negative by the positive ion ejection. Also, the operation of an automatic spacecraft discharge system was to be tested. During the flight EIRMA was to sample the atmosphere and to differentiate between the ambient ions and the energetic ions emitted and created during the vehicle charging and discharging experiments. It also was intended to survey the energy distribution of selected ions.

The instrument was a quadrupole positive ion filter capable of performing a mass scan analysis between 4 and 100 atomic mass units. A mode to detect all positive ions above the atomic mass unit of 80 was also available. To differentiate between the ions at the various energy levels, a program controlled ion retarding potential was available in the instrument.

The capabilities and the physical structure of the instrument were defined by the Ionospheric Disturbances and Modifications Branch. The Branch was also responsible for the design, construction and the packaging of the quadrupole mass filter including the electronics for the excitation signals. The control electronics which accepted and executed the commands from the main controller of the BERT-1 experiment were designed and constructed by the Electronics Research Laboratory of North-

eastern University. The electronics included the communications interface circuits. Circuits to convert the received instructions into the command signals to control the operation of the mass filter and to generate and set the retarding potential also were the responsibility of the Electronics Research Laboratory. Data conditioning and function monitor circuits were also included in the control electronics package.

The first part of this report describes the operation and the interaction between the various circuits during the execution of the commands. The control of the mass filter and the ion retarding potential, as well as the data conditioning processes are also described in this portion of the report. The second part deals with individual circuits and the description of their functions.

## II. OPERATION OVERVIEW

The control circuits for EIRMA were designed to accept digital commands and operating parameters from the master controller of BERT and to convert them into the analog signals to control the operation of the mass filter. Analog control signals were provided to the circuits generating the excitation for the quadrupole and to the high voltage supplies producing the necessary ion retardation potential. The data processing circuits, floating on the retarding potential, amplified the slowly varying ion flux and the mass spectrum signals and converted them into a frequency modulated pulse trains for transmission through optocouplers to the signal conditioning circuits operating at the vehicle potential. There the data was recovered and conditioned for transmission, together with the monitor data, through the telemetry system of BERT. A simplified block diagram of Eirma is shown in Figure 1.



#### A. Command Interface

The commands and the control parameters for EIRMA were stored in the memory of the master controller of BERT. A 16 line parallel bus was used to transfer the required information from the master controller to the control circuits of EIRMA. It was expected that the instruments of BERT ejecting electrons or positive ions from the vehicle would generate large amounts of electromagnetic interference. To minimize the possibility of errors in the control data, due to that interference, the bus was isolated from all of the instruments by optocouplers.

Twelve lines of the bus were used to communicate the commands and the operating parameters to EIRMA. The remaining four were reserved for the transfer control functions. The four MSB's of each 12 bit control word identified the nature and the destination of the data contained in the 8 LSB's. Thus, the data, which defined a single parameter of a task to be performed by EIRMA during the next mode of operation, was stored in an appropriate temporary memory location of EIRMA identified by the 4 MSB's of the control word. When the control word was identified by its MSB's as a command, the LSB's were disregarded. The 16 possible identification codes and the corresponding commands or task parameters are described in the Appendix A.

When EIRMA was ready to accept a new control word, a bus line designated to identify that state (RDY), was set high. After the master controller, at its convenience, placed the new data into the bus, it pulled another one of the transfer control lines low ( $\overline{\text{STR}}$ ). The negative transition on the  $\overline{\text{STR}}$  line was interpreted by EIRMA as a signal that the control word on the bus was stable and ready to be accepted. After the data or the command on the bus was accepted, the RDY line was

pulled low to signal that EIRMA has indeed accepted the data. When EIRMA was ready to accept the next control word, the line was returned to its high state. The data transfer, one control word at a time, could take place while the instrument was executing the tasks commanded during the previous data transfer. Once all of the data for the next mode of operation has been transmitted to EIRMA, an END OF DATA (EOD) command code could be issued by the master controller. Upon the reception of the EOD code EIRMA ignored any further attempts to communicate until the program for the mode interval ordered by the previous data transfers was completed once. This condition was signaled to the master controller by keeping the RDY line low. When the execution of the program has been completed once, the RDY line was set high again. The control circuits, if not commanded otherwise, started to repeat the same mode interval program. At this time, EIRMA again became receptive to instructions and commands. Although any one or all previously transmitted instructions could be reissued, if needed, an EXECUTE command was expected at that point during the experiment. The EXECUTE command transferred the instructions from the interim memory locations, where they had been stored since the reception from the master controller, into the operating memory and started their execution. Once the execution of a program commenced, the new data could be fed to the EIRMA control circuits. When the EOD command was by-passed and a set of new instructions were followed by the EXECUTE command, the presently run program was aborted and the new instructions were executed immediately. Thus, the EXECUTE command provided the synchronization between the events of BERT and the measurements of the mass filter. The EOD command protected, to a large extent, the new instructions and the program

being run, for at least one complete cycle, from the noisy environment created by the experiment.

In the event that the EIRMA controller "crashed" an internal hard-wired circuit reset the controller and executed a default mode program. This condition was signaled to the master controller by pulling yet another designated transfer control line low. A new set of instructions, followed by the EXECUTE command, once again set EIRMA into the desired operation. The fourth of the transfer control lines was used to reset the controller of the EIRMA and thus to order the execution of the default mode program. The reset could also be ordered by a code transmitted over the bus as a command word.

#### B. Exciter Control

Four parameters were required to define an analog signal for the control of the quadrupole exciter during a mass scan. Two instructions defined the beginning and the end levels of a staircase signal generated by an 8 bit digital to analog (D/A) converter. The other two instructions were needed to define the height of the steps in the staircase signal and the time duration spent at each step. All steps within a scan were of the same size. They could be selected to range from one to 255 least significant levels in height. The time spent at each step could be programmed to extend from 0.5 to 127 milliseconds in 0.5 millisecond increments. Regardless of the size of the step increment, a scan always ended on the specified end level or on the full scale output voltage of the D/A converter set at +10 volts. A zero step height or dwell time specification produced a dc output at the specified scan start level. This analog signal controlling the mass scan was accepted by the quadrupole exciter circuits at the vehicle potential.

An additional control parameter associated with the operation of the mass filter defined the ratio between the dc and the ac components of the quadrupole excitation. This parameter controlled the duty cycle of a pulse width modulated waveform. This waveform was transmitted through an optocoupler to the output circuits of the exciter operating at the ion retarding potential. There, the necessary dc component was generated by tapping a portion of the ac component from the output windings of the excitation transformer, passing it through a rectifier and gating the resulting signal into a voltage divider-filter. The pulse width modulated signal from the EIRMA controller was used to generate the gating waveform. The duty cycle of the 8 kHz ratio control signal could be defined with a 6 bit resolution between 21.5% and 78.5% of the period. Codes defining the duty cycle outside of these limits produced a dc ON or a dc OFF at the output of the optocoupler.

#### C. Retarding Bias Control

Two sources could be selected to provide data for the control of the ion retarding bias. One of the sources was a voltmeter measuring the potential of an electrically isolated segment of the vehicle with respect to the main body of the vehicle containing the mass analyzer and other instruments. The other source of control was the data in the program stored in the main controller of BERT.

Since the isolated segment of the vehicle was expected to assume the potential of the surrounding plasma, the voltmeter produced an analog signal which tracked and was proportional to the potential difference between the mass filter and the surrounding plasma. That signal was expected to vary between + and - 10 volts. When this signal was

selected to control the amplitude of the ion retarding bias, it was sampled at the beginning of each EIRMA mode interval or its repetition. The amplitude of the sample determined the output level of the positive HV supply providing the ion retarding bias. Voltages ranging from -100 to +4500 volts could be generated with an approximate resolution of 24 volts. Only the negative signal representing a negative vehicle/plasma potential from the isolated segment voltmeter was thus converted. A sample of a positive signal, regardless of its amplitude, produced a fixed -100V bias.

There were three modes in which the data from the main controller could be utilized to establish the retarding bias. In one of the modes the -100V fixed bias was provided. The second mode selected a fixed positive bias within the limits described in conjunction with the isolated segment voltmeter control. In the third mode, the retarding bias could be scanned between two selected levels in a manner similar to the mass scan control signal. The only difference between the two control signals was in their resolution. While the mass scan had an 8 bit resolution, the retarding potential scan operated with a 7 bit resolution. Since the mass scan and the retarding bias scan were mutually exclusive events, the same codes describing the four control parameters were used for both. A code was assigned to inform EIRMA controller of the role reversal.

A safety feature was included in the control circuits to protect the circuits operating at the high potentials from damage during testing, adjustment and/or calibration. It was a simple measure intended to protect the circuits from a possible damage due to a voltage breakdown at unacceptable gas pressures by preventing an accidental full turn-on of the instrument. When a safety connector was in place,

the maximum amplitude of the retarding potential was limited to below 300 volts. Also, the power to the Channeltron bias and the electrometer supplies was interrupted. A signal was provided to the exciter circuits which was used to limit the amplitude of the ac component of the quadrupole excitation to an acceptable level.

#### D. Data Conditioning

Nine analog data and monitor signals in the range of 0 to +5 volts were provided for transmission through the telemetry system of BERT. Four of the signals carried the principle data, while the other five provided diagnostic monitoring. The ion mass spectrum, the ion flux, mass identification and the ion retarding bias signals were the primary data. The monitors included the Channeltron bias voltage, the quadrupole exciter primary signal amplitude, the temperatures of the exciter and the dc-to-dc converter circuits and the output of a pressure transducer.

Logarithmic current amplifiers were used to convert the ion flux and the ion mass spectrum currents into the voltage signals. The converters were designed to produce a one volt change in the output for each decade of the input current. The expected range of the positive ion flux current was between  $10^{-13}$  and  $10^{-7}$  A, while the ion mass spectral current from the Channeltron was in the  $-10^{-12}$  to  $-10^{-6}$  A range. Since the electrometers operated at the ion retarding bias, the data had to be translated to the vehicle potential for transmission through the telemetry; therefore, the slowly varying outputs of the electrometers were converted into frequency modulated pulse trains and transmitted through optocouplers to the recovery circuits. There the process was reversed. The slowly varying signals were recovered and

presented in an acceptable amplitude range to the telemetry system.

To assist in the identification of the species in the ion mass spectrum, the signal from the digital-to-analog converter controlling the mass scan was attenuated and transmitted as one of the principle signals. The retarding bias and the Channeltron bias were monitored directly using high voltage resistors in the input circuits of operational amplifiers. The other monitor signals were conditioned for telemetry using various operational amplifier configurations as required.

Three external power sources were required:  $\pm 28$  volts and -56 volts. An internal dc-to-dc converter generated the required  $\pm$  and the +5 volts. The exciter needed the two negative voltage batteries in addition to the positive 28 volts. An average current drain from the 28 volt batteries was 300mA. The current from the -56 volt battery averaged 0.5A with a peak of 1.3A at the maximum amplitude of the quadrupole ac excitation signal.

### III. CIRCUITS

The control unit for EIRMA was based on a microcomputer supplemented by CMOS logic. Optocouplers isolated the command bus of BERT from the circuits of EIRMA. Optoisolators were also used where the internal signals had to be transmitted between circuits operating at vastly different reference bias. To convert the digital commands and data into the analog signals required to control the mass filter and the ion retarding bias, monolithic digital-to-analog interface circuits were employed. When feasible, the analog signals were processed by circuits based on quad operational amplifiers. More specialized monolithic circuits such as very low bias current electrometer operational amplifiers and voltage to frequency converters were employed when needed. The circuits were constructed by wirewrapping component

sockets into perforated fiberglass boards. All power converters were commercially available units. The circuits grouped by their natural interaction and/or placement within the confines of EIRMA housing are shown schematically in Figures 2 through 5.

#### A. Control Unit

The control unit of EIRMA is shown in Figure 2. The optocouplers U7, U8, U11 and U12 accepted the input signals from the bus. The four bits ( $A_0 - A_3$ ) carried the commands or the classification codes of the 8 bit data appearing on the lines  $D_0$  through  $D_7$ . The resistor networks RN2 and RN3 limited the bus current to the input diodes of the optoisolators. The current was limited to approximately one mA for each diode. U8 also processed the STROBE pulse, instructing the controller that the data on the bus was stable and was intended for EIRMA. The same unit accepted the external RST (reset) pulse. The READY signal, indicating to the main controller of BERT that EIRMA was ready to receive instructions and the DFLT (default) signal, showing that the default program was controlling the operation of the mass filter, were isolated from the bus by OPI 7010 optoisolators.

The data was accepted, interpreted and the appropriate outputs to control the operation of EIRMA were generated by the single chip microcomputer 8751. The operating program, presented together with the flow charts in Appendix B, was stored in the EPROM of the microcomputer. The external interrupt (pin 13) was programmed to respond on the falling edge of the STROBE pulse. Bits 4 through 7 ( $P2.4 - P2.7$ ) of the I/O port 2 received the data identification code. Data was accepted through the I/O port 1 ( $P1.0 - P1.7$ ). Once the data was accepted, bit 3 of port 2 ( $P2.3$ ) was cleared and, through the CMOS OR gate (U6) serving as



a buffer, turned the diode in the optocoupler OPI 7010 ON to acknowledge the reception of the data. Ten  $\mu$ s later the optocoupler was turned OFF and the READY line was returned to its high state.

Two approaches could be used to reset the microcomputer. For a direct reset, the microcomputer could be accessed from a RST line of the bus through the optocoupler U8 and the gate U13. Also, a reset command could be issued on the bus lines  $A_0$  through  $A_3$ . A code 9H at the outputs of U7 enabled the AND gates U4. The positive strobe pulse from U8 passed through that gate and the OR gates U13 to the reset pin (9) of the microcomputer. An automatic reset was generated within the control unit whenever the microcomputer failed to execute a prescribed routine. When the chip operated within the program, a pulse issued at P3.2 periodically retrigged the monstable U2. The output at  $\bar{Q}$  (pin 7) was in the ZERO state and inhibited the oscillator U3. The output Q (pin 10) of the second monstable in U2 was also reset to ZERO. When the microcomputer failed to trigger the monstable, the output at pin 7 back biased the diode CR1. The oscillator became active. Its output, reshaped into a narrow pulse by the second monostable, propagated through the gates U13 to reset the microcomputer. Once reset, the computer executed the default program to control the operation of EIRMA. The  $\overline{DFLT}$  line on the bus was pulled low to inform the main controller that the default program was controlling the mass filter. The line returned to its high state when new instructions were received from the main controller of BERT and the program for the new mode interval was entered.

The internal digital commands to control the quadrupole exciter and the ion retarding bias were communicated to the digital to analog converters U9 and U10 through the I/O port 0. To boost the

drive capabilities of the port, CMOS buffer U5 and the OR gates U6 were employed. The pull-up resistor network RN1 was used to raise the output levels of the port to the voltages required by the CMOS units. The chip select pulses to latch the data into the appropriate analog to digital converters were generated at P2.0 and P2.1. An 8 bit resolution was used for the control of the exciter, while only the 7 MSB's were used to control the retarding bias. The two MSB's (P0.6 and P0.7) were OR-ed by U6 and presented as the MSB to U10. The ratio control signal, an 8kHz pulse width modulated waveform was produced at P3.1. Pulse widths from 28 to 102 $\mu$ s could be achieved with an approximate 2 $\mu$ s resolution. The MOSFET Q1 was used to drive the diode of an optocoupler which transmitted the waveform to the exciter circuits operating at the ion retarding bias. Bits 4, 5 and 6 of port 3 were used to select the control sources for the ion retarding potential.

#### B. Retarding Bias Control Circuits

The circuits to control the power supplies providing the retarding bias are shown in Figure 3. When the data in the microcomputer was selected to control the retarding bias, a ONE at pin 1 of U6 (VR1) enabled the AND gate and closed the "switch" between the pins 4 and 9 of the analog data selector U7. Thus, the output of the DAC AD558 was connected to the summing junction of the amplifier formed by U8 and the MOSFET Q<sub>1</sub>. R16 served as the feedback resistor of the amplifier. The output of the amplifier provided the power to a high voltage supply (Figure 4) whose output was proportional to the input voltage. A small offset current was injected into the summing junction of the amplifier by R18 and R19 to provide the required minimum input voltage for the supply when the output of the DAC was at zero volts. When the

input of  $Q_2$  (MODE SAFE) was shorted to ground the relay K1 shunted the feedback resistor R16 with R17. The gain of the amplifier was reduced by a factor of 16. Thus, the maximum output voltage of the high voltage supply was limited to approximately 300 volts. Also, the power to the other HV circuits was interrupted (+28V OUT). This safety feature was primarily introduced to prevent voltage breakdown due to an accidental turn-on at reduced pressures. When the relay was in the flight (unsafe) position, +28V were provided to the exciter circuits. There the voltage was used to put the exciter into the full power operation. The dc to dc converter supplying the power to the circuits operating at the retarding bias was also activated. A monitor signal was derived from the +28V by R11 and CR6. This +5V monitor level was passed through an inverter in Figure 2 and continued on as the "SAFEMON" to become a part of a more complex monitor signal in Figure 5.

Since the two MSB's of the microcomputer output were OR-ed into the MSB of the DAC controlling the retarding bias, the output of the DAC reached the full scale value when 7FH were latched into the unit. When the input to the DAC was increased to 80H, the output of the DAC dropped to a half scale value, from where it could be increased back to the full scale value when the digital input reached BFH. The same process repeated itself for inputs between COH and FFH. The MSB of the data was also latched into the pin 13 of U2. When the MSB was a ONE, the outputs of U6 and U5 were driven high. The MOSFET  $Q_3$  turned ON an optoisolator, which in turn switched in a supply floating on the output of the supply controlled by the DAC, (Figure 4). The combined output of the two provided the required retarding bias. Thus, at an input of 7FH two thirds of the full scale output was generated by

the non-floating supply. At 80H again an output of two thirds was generated, but this time by the combined efforts of both supplies. From there, the full scale output could be obtained by increasing the contribution of the ground base supply.

When the isolated sector voltmeter was selected to control the retarding bias, the inverted analog signal at the output of U1 (pin 1) was converted into a digital signal by U3. The conversion was triggered by the selection signal VR2 originating at the microcomputer. The digital word was reconverted into an analog output by U4 which completed the digital sample and hold circuit. As in the previous case, where the microcomputer controlled the retarding bias, the two MSB's of the digital word were OR-ed. The MSB also controlled the status of the transistor  $Q_3$  through the gate U5, provided pin 13 of U6 was high. The status of that pin was determined by the polarity of the isolated segment voltmeter. When the output of the voltmeter was positive, a ZERO was latched into the pin 2 of U2 by the VR2 signal. The AND gate U6 (pin 13) was disabled. A negative signal from the voltmeter enabled that gate. The enabling signal also controlled the status of the switches in U7. When U6 was enabled the switch connecting pins 3 and 9 of U7 was closed. The output of the digital sample and hold circuit was connected to the amplifier U8. The signal generated by the amplifier at the drain of  $Q_1$ , using the data derived from the voltmeter, could be modified by the output of the AD558 DAC. The output of the DAC was attenuated by a factor of 5 at pin 8 of U1 before being summed with the voltmeter signal at pin 3 of U8.

If the output of the isolated segment voltmeter was positive when sampled, the transmission gates in U7 between pins 2 and 9 and 14 and

10 were closed. The input voltage to the HV supplies was reduced to zero. Thus, the supplies were forced to shut down. Pin 2 of U2 was reset to ZERO and since VR1 was at ZERO (deselected) the output at pin 10 of U6 was also forced into the ZERO state. This state closed the relay contacts (shown in Figure 4) and applied a negative bias voltage with respect to the vehicle to the front end of the instrument. That bias could also be selected directly by the computer providing a ZERO at pin 9 of U6 (VR3).

### C. HV and Data Circuits

The high voltage (HV) bias and the data circuits are shown in Figure 4. The circuits include the ion retarding bias supplies, the Channeltron bias supply and the front end bias relay. Also included are the electrometer amplifiers that were employed to measure the ion flux and the mass spectral data gathered at the retarding bias. They were housed within the same pressurized enclosure as the HV supplies.

Two  $\pm 15V$  dc to dc converters (946) provided the necessary power to the circuits floating on the ion retarding bias. These converters could withstand the large voltage differences between the batteries referenced to the vehicle potential and the floating circuits. One of the converters was assigned to provide power to the floating high voltage supplies, while the other powered the data circuits. The power to the floating Channeltron supply K30Z (3000 V max output) was provided through an operational amplifier arrangement of U1 and the MOSFET  $Q_1$ . The output of the supply was fed back through R8 to the summing junction of the combination. The Channeltron bias level was set by the potentiometer R3.

The floating K15Z supply boosted the amplitude of the ion retarding bias (VR). It was provided with the maximum allowed input voltage

of 15 volts through the switch  $Q_2$  and produced 1500V output when activated. The switch was controlled through the optoisolator (OPTO 3) by the control circuits previously described. The K30Z supply referenced to the vehicle potential (ground) provided the controlled portion of the retarding voltage. When a fixed negative retarding bias was needed, the power to the HV supplies K30Z and K15Z was interrupted. The -100 volt unit PS8100 floating on the -56 volt battery provided the necessary bias through R11. The diodes CR2, CR2A and CR3 prevented an excessive attenuation of the negative retarding bias by isolating it from the various resistances to ground. CR2 served yet another purpose. The output of the controlled K30Z retarding bias supply could be reduced only to a minimum of approximately +200 volts before it reached a point of marginal operation. Therefore, to achieve a controlled retarding bias below that minimum, the CR2 diode was chosen to be a low leakage 200 volt zener. Thus, by exceeding the zener voltage at the output of the supply, retarding voltages in tens of volts could be generated. The zener, of course, reduced the maximum achievable retarding bias by its voltage drop to 4300 volts.

The front end bias was also obtained from the fixed negative power supply-battery combination. The signal could be attenuated by  $R_{13}$  and  $R_{14}$ , if needed, before passing through the relay K1. The relay was kept in the active open state and was released to close by the bias control circuit when the mode designated as VR3 was selected (Figure 3).

The magnitudes of the ion retarding bias and the Channeltron bias were monitored. High voltage 100M resistors were used to derive currents proportional to the amplitudes of the voltages. The diodes placed in series with the resistors to prevent excessive loading of the

negative voltage retarding signal also prevented monitoring of that signal. Since the monitored Channeltron voltage was composed of the retarding signal and the negative Channeltron bias, the monitor current was reduced to a very low leakage current of the diode when the magnitude of the positive retarding bias was smaller than the magnitude of the Channeltron bias voltage. To protect the circuits that processed the monitor currents, both monitor resistors were terminated by diodes connected to the vehicle potential.

The electrometer amplifiers U2 and U4 were configured into logarithmic current to voltage converters. The amplifier U2 accepted the negative current from the Channeltron representing the ion mass spectrum, while the U4 unit operated on the positive current produced by the ion flux into the instrument. Both circuits converted 6 decades of input current into a 6 volt output variation. The ion flux meter measured currents in the  $10^{-13}$  to  $10^{-7}$  A range, while the spectrum amplifier accepted currents of  $-10^{-12}$  to  $-10^{-6}$  A. Both amplifiers had similar configurations and differed primarily in the values and the polarity of components selected to accommodate the directions and the range of the input currents.

Dual high gain transistor  $Q_5$  placed in the feedback path of the electrometer amplifier served as the log element. The transistor with its collector connected to the input accepted the current and performed the classical logarithmic current to voltage conversion. The other transistor within the package reduced the voltage pedestal and thus eliminated, to a large extent, the influence of the reverse saturation current on the result. The operational amplifier (U3) circuit forced a comparatively large constant current (200 $\mu$ A) to flow in the collector,

and consequently, in the emitter of the second transistor. The resistor divider formed by  $R_{27}$ ,  $R_{28}$  and  $R_{29}$  determined the gain of the amplifier. The temperature influence on the signal due to the variation of the junction voltage was minimized by the sensor  $R_{28}$ . To speed the recovery of the circuit from a cut-off state caused by the input current reversals generated by the transients in the system, a circuit to inject a current into the input was used. The voltage divider formed by  $R_{24}$ ,  $R_{25}$  and  $R_{26}$ , together with the transistor  $Q_{12}$  diverted the unwanted current from the input whenever the output of the amplifier (U2) was forced to go below a preset level.

The output of the logarithmic circuit was inverted and then converted into a frequency modulated pulse train by the circuit of U5. The modulated data signal was passed through the optocoupler (OPTO 1) and reshaped at the vehicle potential by the transistor  $Q_{10}$ . The operation of the circuit amplifying the positive ion flux current was very similar to the operation of the mass spectra amplifier just described.

#### D. Signal Conditioning and Monitor Circuits

The reshaped frequency modulated pulse trains, carrying the data processed by the electrometers, were reconverted into the slowly varying signals by the converter circuits shown in Figure 5. Also shown are the amplifiers processing the monitor currents derived from the retarding potential and the Channeltron circuits. In addition, signal conditioning circuits for the temperature and the pressure transducer data, the exciter signal monitor and the "safe" state indicator were located on the same board and are included in the drawing.

The frequency to voltage converter circuits U5 and U6 used to recover the ion mass spectrum and the ion flux data were identical. To



establish the zero volts reference for the data signals, appropriate offset currents were injected into the summing junctions of U4 (pins 2, 9). The currents were derived from the voltage reference source  $O_1$  through the voltage inverter U3 and the resistors  $R_{41}$  and  $R_{42}$ . Potentiometers  $R_{40}$  and  $R_{43}$  provided the adjustment capability. The gain, to establish the 5 volt full scale limit for the data acceptable to the telemetry circuits, could be trimmed with the potentiometers  $R_{39}$  and  $R_{46}$  located in the feedback loops of the amplifiers. The remaining harmonics generated during the frequency to voltage conversion were removed from the signal by the two pole low pass output filters. To protect the telemetry circuits from possible overvoltages, the outputs of the filters were limited to a maximum of 5.6 volts by the CR11 and CR12 diodes.  $R_{60}$  and  $R_{61}$  converted the generated data signals from a one volt per decade to 0.9V per decade to accommodate approximately 6 decades of data within the 0 to 5 volt range of the telemetry signal.

The monitor current derived from the retarding potential was converted into a voltage by U1 (pin1). The output, representing 1000 volts of retarding potential per volt, was passed through an inverter and a voltage limiter before proceeding to the telemetry circuits. The small offset introduced by  $R_4$  accounted for the voltage loss in the 200V zener placed in the path of the retarding potential (Figure4). The resistor could be removed when the retarding voltage and not the supply voltage was to be monitored. Also, the output of U1(pin1) was summed with the monitor current derived from the Channeltron bias circuit. This operation removed the contribution of the retarding potential signal to the Channeltron bias monitor current. Therefore, only the Channeltron bias voltage was represented by the signal ( $V_E$ ) sent through the telemetry.

Two temperature sensors LM235 were included with the confines of EIRMA. One of these was located with the exciter circuits (RF TEMP) while the other (CR4A) monitored the temperature of a dc to dc converter supplying power to the control and the data circuits operating at the vehicle potential. The sensors produced an increment of 10mV for a change of one  $^{\circ}\text{C}$  in the temperature. The offset current through  $R_9$  ( $R_{15}$ ) established a zero volt output at 25 $^{\circ}\text{C}$ . The maximum temperature was expected to be below 75 $^{\circ}\text{C}$ . It was represented by a full scale output of 5 volts. The dc to dc converter temperature monitor signal was processed in combination with the safe mode indicator. As previously stated, the safe mode limited the operation of the quadrupole exciter and the HV bias circuits to the output levels below the voltage breakdown limits in a partial vacuum. When in the safe mode, the dual JK flip-flop U8 was kept in the reset state by a ONE on the SAFE MODE signal line. The diodes CR6 and CR7 were cut-off. The signal from the temperature sensor CR4A was conditioned by the circuits of U2 and appeared as a dc level at the cathode of the amplitude limiter diode CR5A. When EIRMA was in the flight ready mode, the JK flip-flop U8 connected as a modulo-3 counter, was released from the reset state by a ZERO on the SAFE MODE line. The 8kHz ratio control signal (from Figure2) scaled to approximately one Hz by U7( $Q_{13}$ ) triggered the flip-flop. In its sequence, the flip-flop first forward biased CR7 and pushed the output of the amplifier U2 beyond +10 volts. This forced the diode CR6A to limit the output to +5 volts. Next, both diodes CR6 and CR7 were cut-off. In this state the output of the amplifier was determined by the temperature sensor CR4A. In its third state, the flip-flop forward biased CR6 and forced the output of the amplifier into the negative direction. The negative excursion was limited by

CR4 to one diode drop. Thus, the signal to the telemetry system was kept at zero volts. This sequence, repeated once every 3 seconds, could be used to caution the operator that EIRMA was fully operational.

The pressure transducer Syncom model LX1603A was located in the exciter section. It monitored the pressure in the exciter and the HV circuit enclosures which were interconnected. Since the output of the transducer could range between 2.5 and 12.5 volts, its signal was first offset by -215 volts and then attenuated by a factor of 2 in the circuits of U3.

An additional signal originating in the exciter section was processed by the monitor circuits. This signal representing the amplitude of the ac excitation at the primary of the transformer was attenuated and limited by U1 and CR9 before being passed on to the telemetry.

#### IV. APPENDIX A

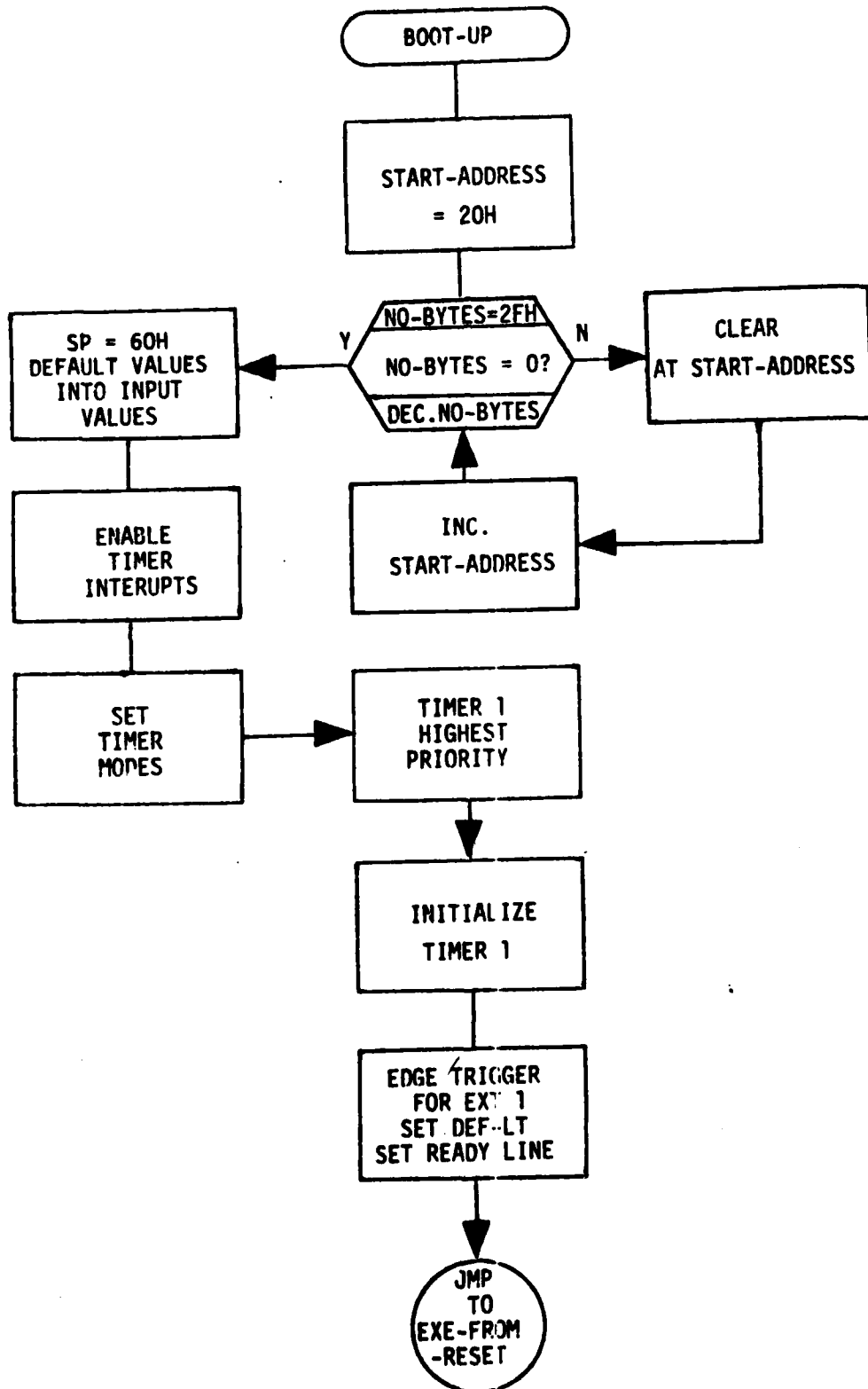
##### EIRMA CONTROL CODES

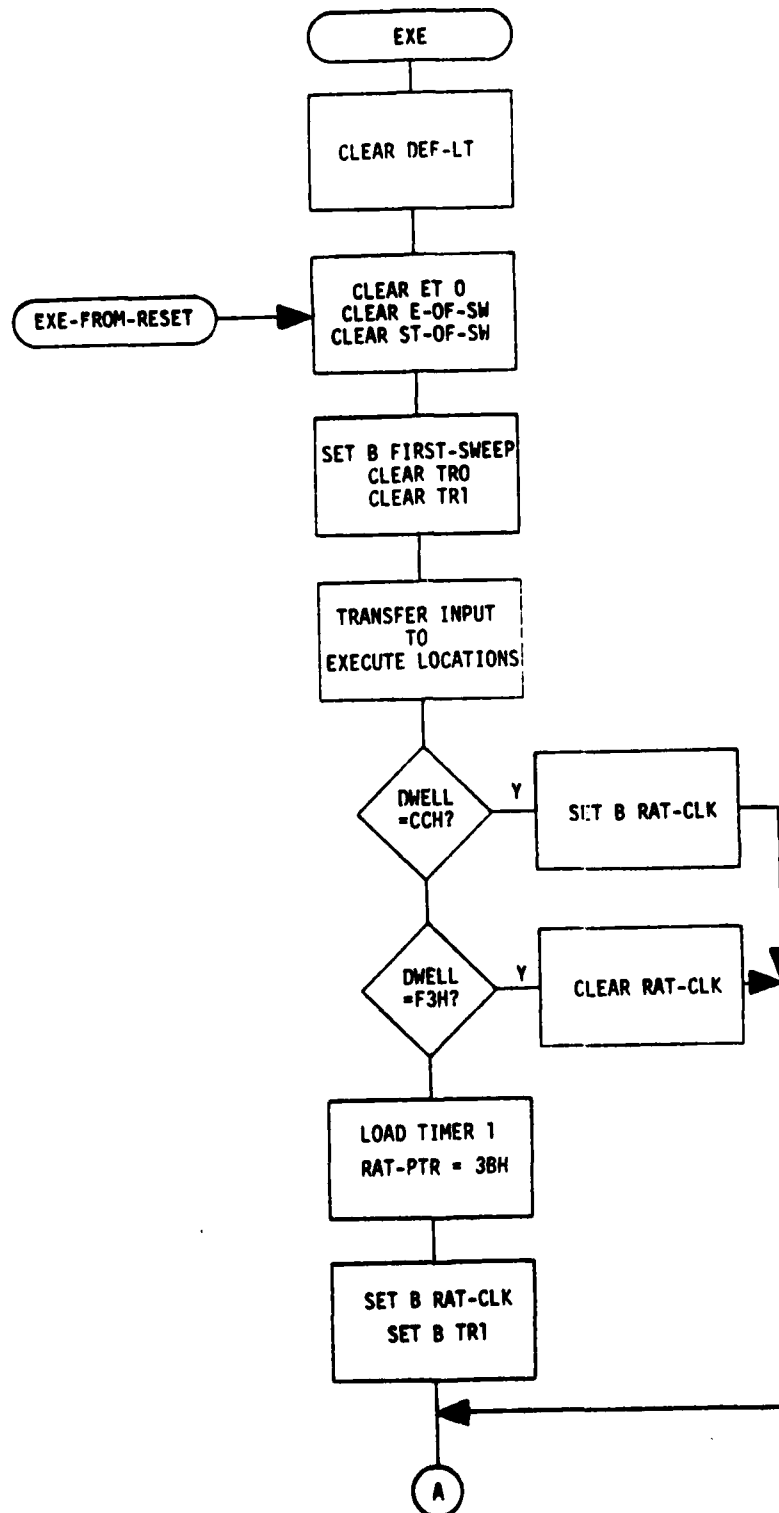
1. 00H - Address code followed by an 8 bit data code specifies the starting point of an AMU sweep.
2. 01H - Code in conjunction with an 8 bit data code determines the end point of the AMU sweep.
3. 02H - Together with the 8 bit data code specifies the number of levels (0 to 255) by which the AMU sweep control signal is incremented during a sweep. The sweep ends at the point specified by the accompanying data of the 01H code, regardless of the size of the last increment which could cause an overshoot if executed. A ZERO stops the sweep.
4. 03H - And the 8 bit code specifies the time interval spent at each AMU sweep increment. The DWELL TIME =  $0.5(FF-NN)H$  nS. Where  $0 < NN < FF$  is the 8 bit data code. A ZERO stops the sweep.
5. 04H - Spare
6. 05H - Code and the three (3) LSB's of the accompanying data select the ion retarding potential control source. The LSB (BIT 0) transfers control to the digital data transmitted in conjunction with the 06H code. The NLSB selects the isolated segment voltmeter output as the control signal. Bit 2 replaces the positive variable high voltage supply with a fixed voltage of -156 volts as the source of the retarding potential. Only one bit at a time may be designated as ONE.
7. 06H - Code and the 8 bit data code determine the output level of the retarding potential source when the digital data stored in the program is selected as the control source by the code 05H.
8. 07H - Spare
9. 08H - Code forces EIRMA controller to interpret the codes 00H through 03H and the accompanying data as the ion retarding potential control codes and the data identified by 06H code as the AMU level definition.
10. 09H - Code in conjunction with the STROBE (STR) signal generates a RESET command for the EIRMA controller. The controller switches into the default program.

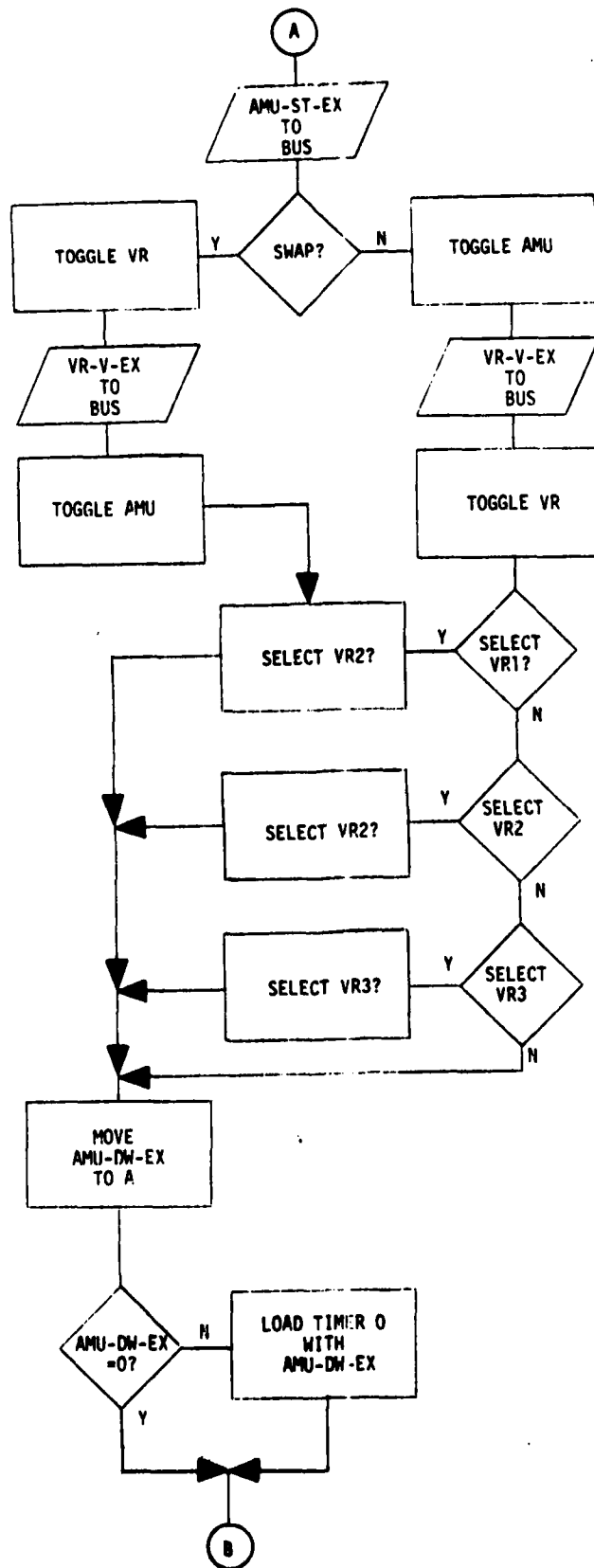
#### APPENDIX A (continued)

- 11. OAH - Code and the six (6) LSB's of the data code determine the duty cycle of the signal controlling the ratio between the ac and the dc components of the quadrupole excitation signal. Data between 00H and 0CH produce a dc level which turns the ratio control optoisolator input LED ON. Data 33H through 3FH turn the LED OFF. Data 0DH through 32H produce positive (LED ON) pulse widths ranging from 102 to 28 $\mu$ s while maintaining the period of approximately 130 $\mu$ s.
- 12. OBH - Reserved for internal use.
- 13. OCH - Spare
- 14. 0DH - End of data designator (EOD).
- 15. OEH - Starts the execution of the new mode interval program. (EXECUTE)
- 16. OFH - Reserved for internal use.

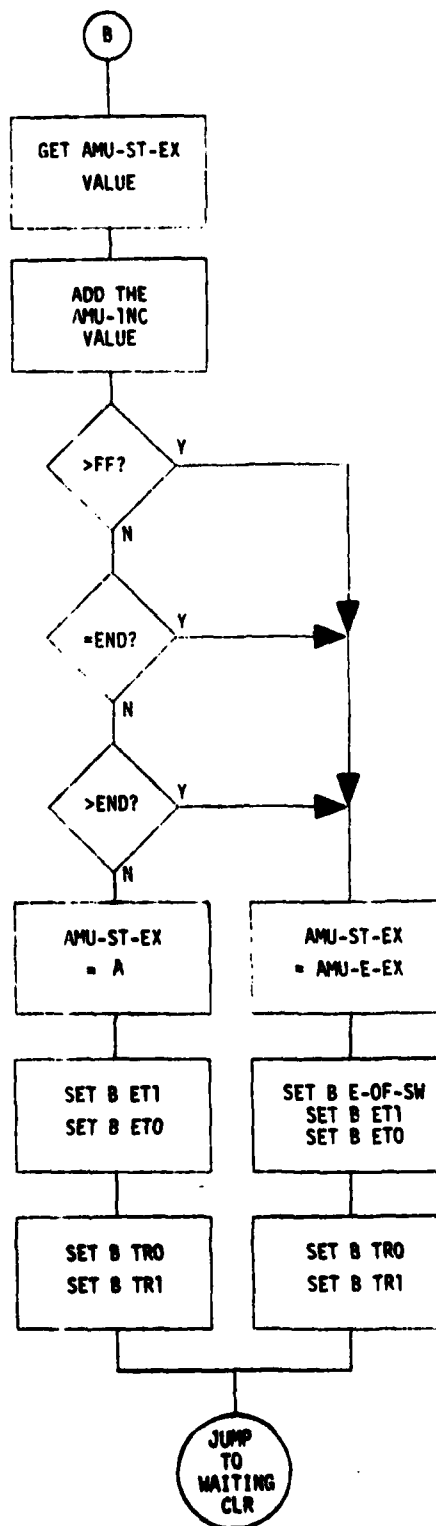
V. APPENDIX B  
FLOWCHARTS AND PROGRAMS

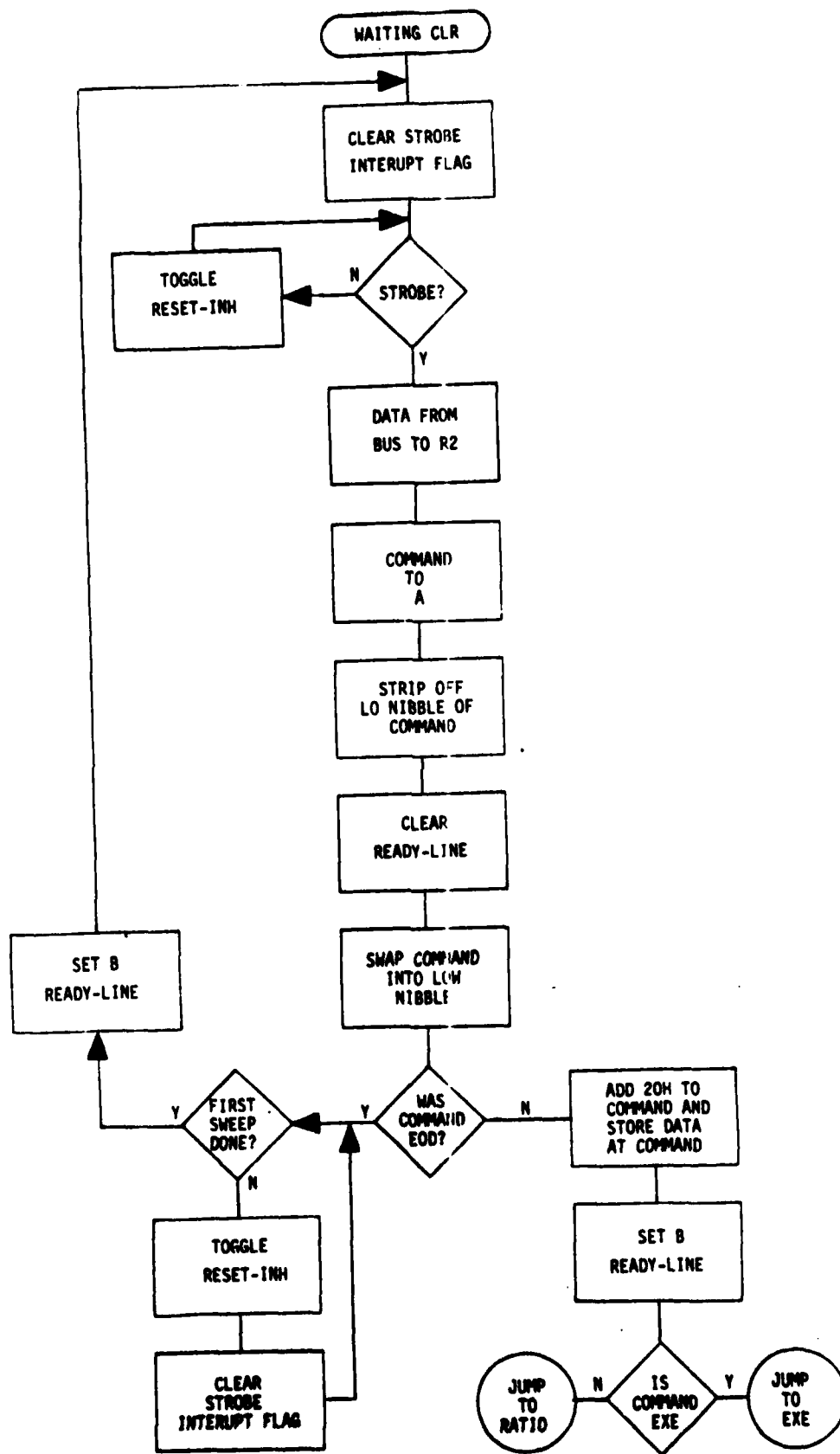


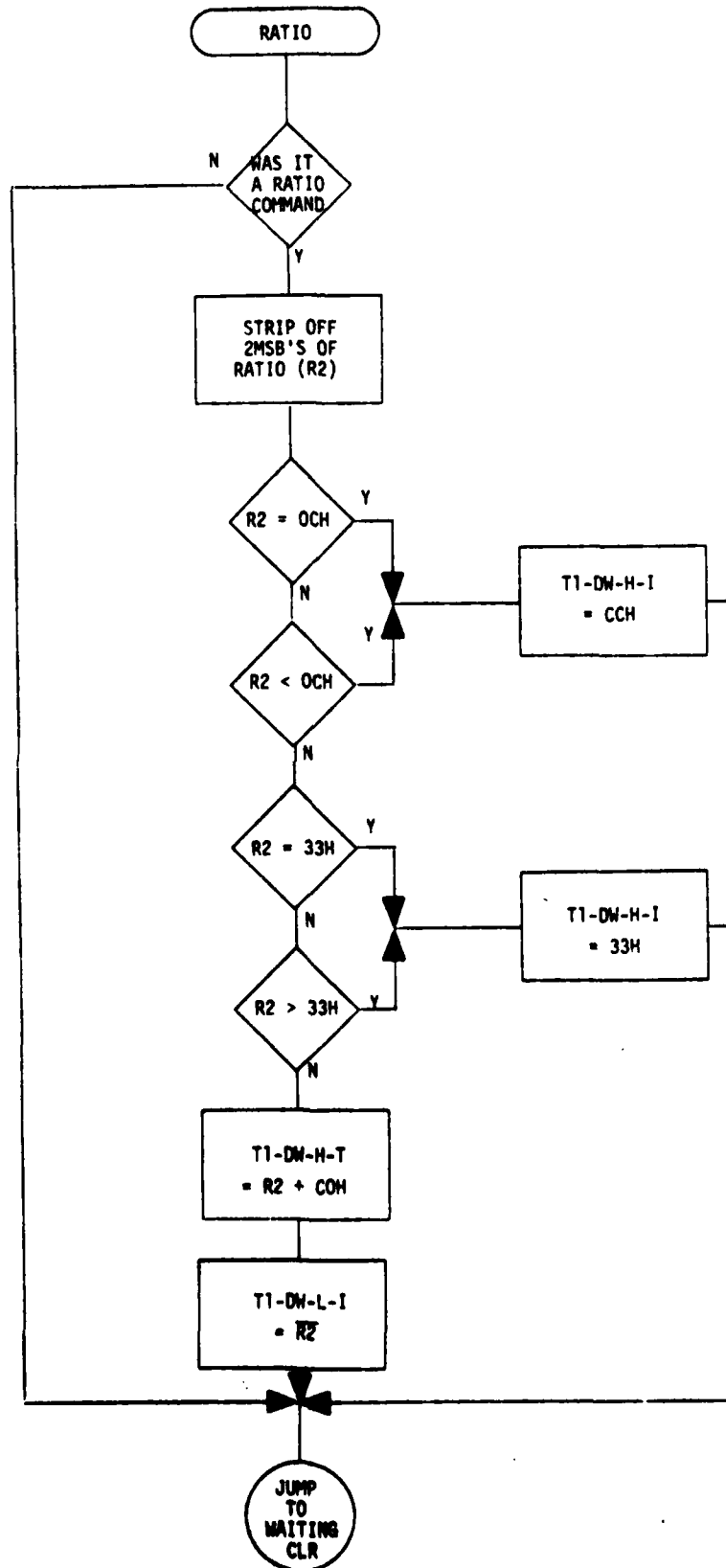


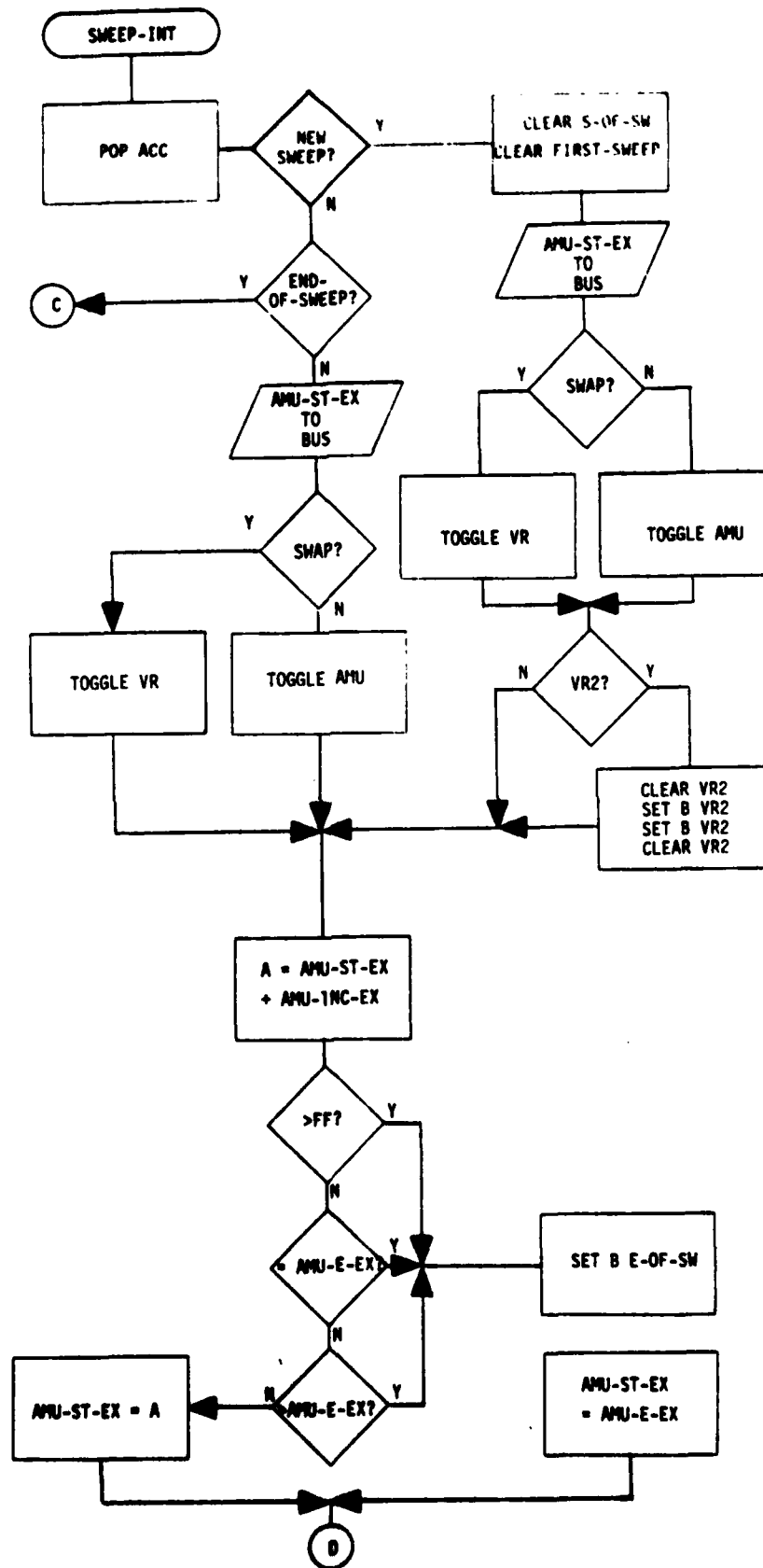


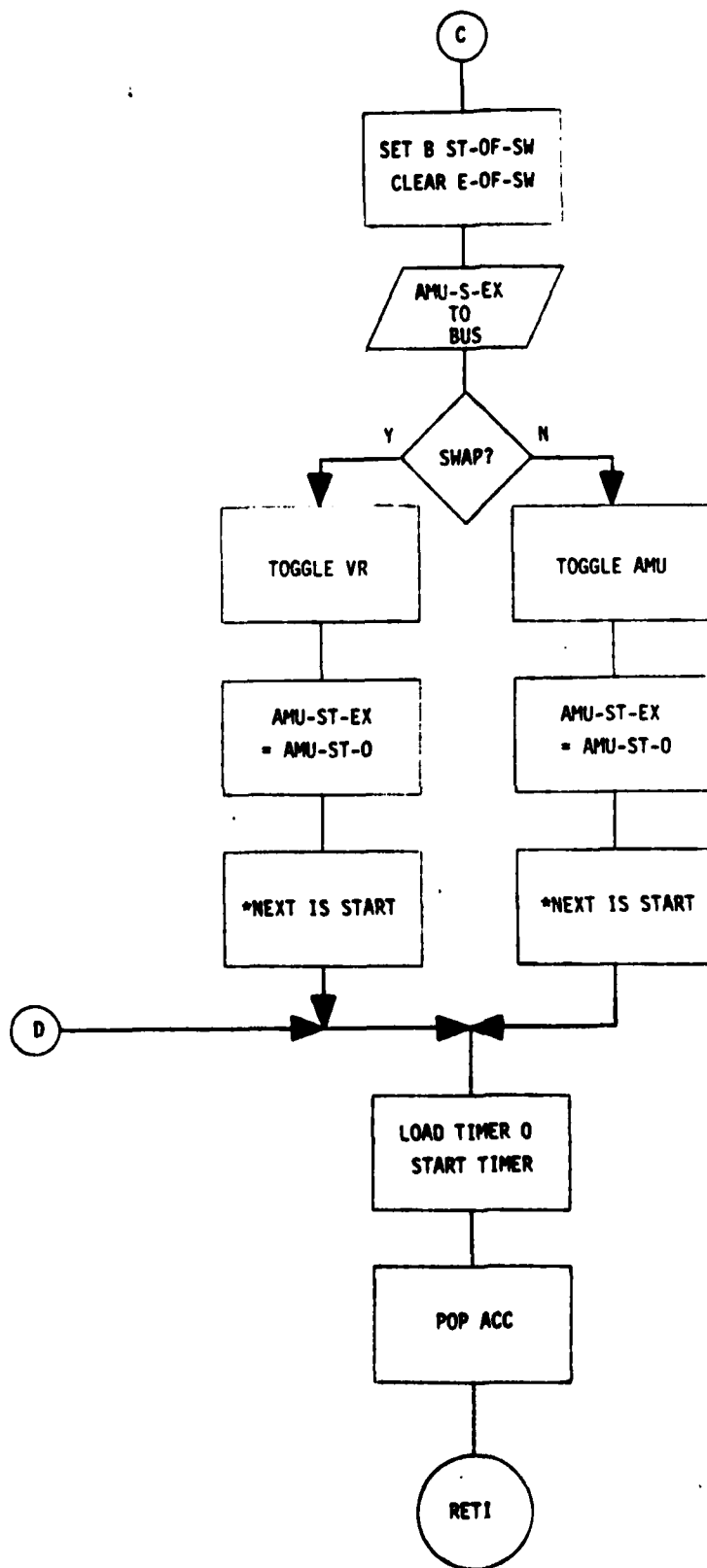


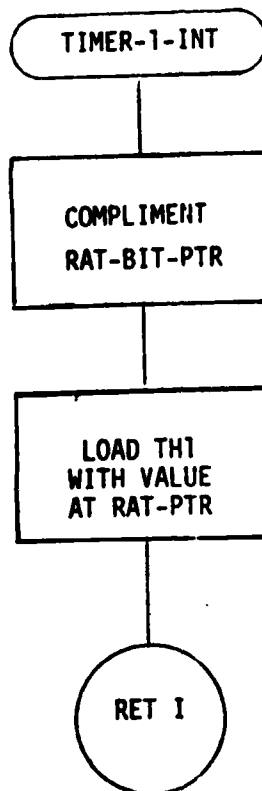












ISIS-II MOS-51 MACRO ASSEMBLER V2.1  
 OBJECT MODULE PLACED IN :F1:EIR.OBJ  
 ASSEMBLER INVOKED BY: :F1:ASM51 :F1:EIR.SRC

LOC	OBJ	LINE	SOURCE
		1	\$TITLE(EIRMA AMU/VR CONTROLLER)
		2	\$DATE(4/11/85)
		3	\$DERUS
		4	\$PAGELENGTH(55)
		5	\$XREF
		6	\$NOSEN
		7	\$EB
		8	\$INCLUDE(:F1:EIR.DEF)
		9	;
		10	;
		11	;
		12	;*****
		13	;;
		14	;; EIRMA MEMORY AND DEFINITION SECTION
		15	;;
		16	;*****
		17	;
		18	;
		19	;; DEFAULT NAMES
0080		20	BUS EQU R0
0040		21	COMMAND EQU R2
0090		22	DATA_BUS EQU R1
		23	;
		24	;
		25	;; DEFAULT VALUES
0018		26	AMU_ST_D EQU 16H
0070		27	AMU_E_D EQU 70H
0001		28	AMU_INC_D EQU 01H
00F4		29	AMU_DW_D EQU 0F4H
0004		30	VR_S_D EQU 04H
0000		31	VF_V_D EQU 00H
00CF		32	T1_DW_H_D EQU 0CFH ; VALUE = VALUE AS FROM CONTROLLER + 0CFH
00F0		33	T1_DW_L_D EQU 0F0H ; VALUE = CPL OF VALUE AS FROM CONTROLLER
		34	;
		35	;
		36	;; MEMORY LOCATIONS
		37	;
		38	;
		39	;; E-END
		40	;; I-INPUT
		41	;; S-SELECT
		42	;; ST-START
		43	;; EX-EXECUTE
		44	;; O-OPERATIONAL
		45	;; V-VALUE

```

LBC OBJ      LINE      SOURCE
              =1 46      ;
              =1 47      ;
0020          =1 48      AMU_ST_I      DATA 20H
0030          =1 49      AMU_ST_EX     DATA 30H
0034          =1 50      AMU_ST_O      DATA 34H
0021          =1 51      AMU_E_I      DATA 21H
0031          =1 52      AMU_E_EX     DATA 31H
0022          =1 53      AMU_INC_I     DATA 22H
0032          =1 54      AMU_INC_EX    DATA 32H
0023          =1 55      AMU_DW_I      DATA 23H
0033          =1 56      AMU_DW_EX     DATA 33H
              =1 57      ;
              =1 58      ;
0025          =1 59      VR_S_I        DATA 25H
0035          =1 60      VR_S_EX       DATA 35H
0026          =1 61      VR_V_I        DATA 26H
0036          =1 62      VR_V_EX       DATA 36H
              =1 63      ;
              =1 64      ;
002F          =1 65      RAT_PTR       DATA 2FH
              =1 66      ;
              =1 67      ;
002A          =1 68      T1_DW_H_I     DATA 2AH
002B          =1 69      T1_DW_L_I     DATA 2BH
003A          =1 70      T1_DW_H_EX    DATA 3AH
003B          =1 71      T1_DW_L_EX    DATA 3BH
              =1 72      ;
              =1 73      ;
              =1 74      ; BIT LOCATIONS
00B4          =1 75      VR1           BIT 0B4H ;PORT 3.4
00B5          =1 76      VR2           BIT 0B5H ; 3.5
00B6          =1 77      VR3           BIT 0B6H ; 3.6
00B7          =1 78      DEF_LT        BIT 0B7H ; 3.7
00A0          =1 79      AMU           BIT 0A0H ;PORT 2.0
00A1          =1 80      VR            BIT 0A1H ; 2.1
00A2          =1 81      READY_LINE    BIT 0A2H ; 2.2
0079          =1 82      RAT_BIT_PTR   BIT 79H ;BIT 0 IN LOC. 2F (T1 DWELL VALS.)
00B1          =1 83      RAT_CLK       BIT 0B1H ;PORT 3.1
00F0          =1 84      ST_OF_SW      BIT 0F0H ;START OF SWEEP FLAG
00F1          =1 85      E_OF_SW       BIT 0F1H ;END OF SWEEP FLAG
00F2          =1 86      FIRST_SWEEP   BIT 0F2H ;SWEEP HAS JUST STARTED FROM EXE
00B3          =1 87      STROBE        BIT 0B3H ;STROBE PIN
00B2          =1 88      RESET_INH     BIT 0B2H ;RESET INHIBIT PIN (PREVENT AUTO RESET)
00F3          =1 89      EYE_INT       BIT 0F3H ;FLAG THAT THIS WASNT A REAL INT (FROM EYE COM)
              =1 90      ;
              =1 91      ;
              =1 92      $INCLUDE('F1:RAM0.MAC')
              =1 93
              =1 94      $DEFINE(RAM_CLR(START_ADDR,NO_BYTES)) LOCAL SET_TO_ZER
              =1

```



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```

LOC 000      LINE      SOURCE
=1              %' TOGGLES A BIT/PIN WRITTEN 10/84
=1              %'
=1              CLR    %BIT_ADDR    %'BRING PIN/BIT LOW'
=1              SETB   %BIT_ADDR    %'RETURN IT HIGH'
=1              %'
=1              %'
=1              )
=1 101          $INCLUDE(=F1:SELVR1.MAC)
=1 102          %DEFINE(SELECT_VR1) (
=1              %'=====Z'
=1              %'                                SELECT VR1 MACRO                                %'
=1              %'=====Z'
=1              CLR    VR2          %'DESELECT VR2 %'
=1              SETB   VR3          %'          VR3 %'
=1              SETB   VR1          %'SELECT VR1 %'
=1              )
=1 103          $INCLUDE(=F1:SELVR2.MAC)
=1 104          %DEFINE(SELECT_VR2) (
=1              %'=====Z'
=1              %'                                SELECT VR2 MACRO                                %'
=1              %'=====Z'
=1              CLR    VR1
=1              SETB   VR3
=1              CLR    VR2          %' VR2 IS EDGE TRIGGER %'
=1              SETB   VR2
=1              SETB   VR2
=1              CLR    VR2
=1              )
=1 105          $INCLUDE(=F1:SELVR3.MAC)
=1 106          %DEFINE(SELECT_VR3) (
=1              %'=====Z'
=1              %'                                SELECT VR3 MACRO                                %'
=1              %'=====Z'
=1              CLR    VR2          %'DESELECT VR2 %'
=1              CLR    VR1          %'          VR1 %'
=1              SETB   VR1
=1              CLR    VR1
=1              CLR    VR3          %'SELECT VR3 %'
=1              )
=1 107          USING 0
=1 108          CSEG AT RESET
=1 109          AJMP    BOOT_UP
=1 110          ORG TIMER0
=1 111          AJMP    SWEEP_INT
=1 112          ORG TIMER1
=1 113          AJMP    TIMER_1_INT
=1 114          ;
=1 115          ;
=1 116          ;
=1 117          ORG 30H

```

```

LOC 080      LINE    SOURCE
              118      ;
              119      BC T_UP:      ZRAM_CLR(*20H,*1FH)
              127      ZDEFPAR
              143      ZTEMP_TO_EXE
006F 758160    159      MOV      SP,*60H
0072 75486A    160      MOV      IE,*8AH      ;ENABLE TIMER INTERRUPTS
0075 758604    161      MOV      TCON,*04H      ;SET EDGE TRIGGER FOR EXT 1 INTERRUPT
0078 758921    162      MOV      TMOD,*21H      ;SET TIMERS TO=MODE 1:16 BIT COUNTER
              163      ;                      T1=MODE 2:8 BIT RELOAD
007B D2B8      164      SETB     IP.3      ;SET PRIORITY FOR TIMER1
007D 793A      165      MOV      R0,*3AH      ;SET UP R0 FAT_PTR
007F 853B9B    166      MOV      TL1,T1_DW_L_EX ;SET UP TIMER1
0082 853ABD    167      MOV      TH1,T1_DW_H_EX
0085 D2B7      168      SETB     DEF_LT      ;LIGHT UP DEFAULT LED
0087 D2A3      169      SETB     READY_LINE
0089 01C4      170      AJMP     EXE_FROM_RESET
              171      ;
              172      ;
008B 00        173      NOP
008C 00        174      NOP
008D 00        175      NOP
008E C2B8      176      WAITINGCLR: CLR IE1
0090 20B806    177      WAIT:  JB      IE1,INPUT      ;ON EDGE TRIGGER GO TO INPUT ROUTINE ***JBC
              178      WAITING: ZTOGGLE(RESET_INH)
0097 80F7      182      SJMP     WAIT
0099 4A90      183      INPUT: MOV     R2,DATA_BUS      ;SET DATA OFF THE BUS
009B E5AC      184      MOV      A,COMMAND      ;ALONG WITH THE COMMAND ASSOCIATED
009D 54F0      185      ANL      A,*0F0H      ;STRIP OFF THE LOW NIBBLE
009F C2A3      186      CLR      READY_LINE      ;ACCEPT ALL DATA SO READY=FALSE
00A1 C4        187      SWAP     A
00A2 B43D0F    188      CJNE     A,*0DH,NOT_EOD ;IS IT AN EOD COMMAND?
00A5 30F208    189      EOD:   JNB      FIRST_SWEEP,EOD_EXIT
              190      ZTOGGLE(RESET_INH)      ;PREVENT AUTO-RESET
00AC C2BE      194      CLR      IE1
00AE 80F5      195      SJMP     EOD
00B0 D2A3      196      EOD_EXIT: SETB  READY_LINE
00B2 30DA      197      SJMP     WAITINGCLR
              198      ;
              199      ;
00B4 2420      201      NOT_EOD: ADD     A,*20H      ;GET THE STORAGE LOCATION FROM THE COMMAND
00B6 F9        202      MOV      R1,A
00B7 A702      203      MOV      @R1,*02H      ;AND USE IT TO STORE R2 (DATA)
00B9 D2A3      204      SETB     READY_LINE      ;SHOW THE DATA ACCEPTED
00BB B42E02    205      CJNE     A,*2EH,NOT_EXE ;WAS IT AN EXECUTE COMMAND?
00BE 8002      206      SJMP     EXE
00C0 2188      207      NOT_EXE: AJMP  RATIO      ;IF IT WASNT IT MUST HAVE BEEN RATIO COMM
00C2 C2B7      208      EXE:   CLR      DEF_LT      ;NO LONGER THE DEFAULT PARAMETERS
00C4 C2A9      209      EXE_FROM_RESET: CLR  ETO
00C6 C2F1      210      CLR      E_OF_SW

```

LOC	ORG	LINE	SOURCE
00C8	02F0	211	CLR ST_OF_SW
00CA	02F1	212	SETB FIRST_SWEEP
00CC	028C	213	CLR TR0
00CE	028E	214	CLR TR1 ;DISABLE TIMERS
00D0	02A9	215	CLR ET0
00D2	02AB	216	CLR ET1
		217	ZTEMP_TO_EXE ;TRANSFER THE INPUT TO THE EXE LOCATIONS
00EF	E53A	233	MOV A,T1_DW_H_EX ;
00F1	B4CC04	234	CJNE A,#00CH,RAT_NOT_CC ;IS THE DWELL=00CH
00F4	02B1	235	SETB RAT_CLK ;IF YES
00F6	8014	236	SJMP STRT_TIMER
		237	;
		238	;
00F8	B4F304	239	RAT_NOT_CC: CJNE A,#0F3H,RAT_NOT_F3 ;RATIO=F3H?
00FB	02B1	240	CLR RAT_CLK ;SET UP RAT_CLK PIN TO PROPER LEVEL (=F3)
00FD	800D	241	SJMP STRT_TIMER
		242	;
		243	;
00FF	853B8B	244	RAT_NOT_F3: MOV TL1,T1_DW_L_EX ;MOVE EXECUTE VALUE INTO T1 LOW
0102	853ABD	245	MOV TH1,T1_DW_H_EX ; HI
0105	752F3E	246	MOV RAT_PTR,#3BH ;SET UP POINTER FOR NEXT INTERRUPT
0108	02B1	247	SETB RAT_CLK ;SET UP RAT_CLK PIN TO PROPER LEVEL
010A	028E	248	SETB TR1 ;START TIMER!
010C	853080	249	STRT_TIMER: MOV BUS,AMU_ST_EX ;PUT START VALUE ONTO BUS
010F	E575	250	MOV A,VR_S_EX ;CHECK IF SWAP IS IN EFFECT
0111	20E310	251	JB 0E3H,VR_AMU_SWAP;IF SO JUMP
		252	ZTOGGLE(AMU)
0118	853680	256	MOV BUS,VR_V_EX
		257	ZTOGGLE(VR)
011F	30E015	261	JNB 0E0H,NOT_VR1
0122	800B	262	SJMP SV1
		263	;
		264	;
		265	VR_AMU_SWAP: ZTOGGLE(VR)
0128	853680	269	MOV BUS,VR_V_EX
		270	ZTOGGLE(AMU)
		274	SV1: ZSELECT_VR1
0135	801E	282	SJMP VR_SELECTED
		283	;
		284	;
0137	30E10E	285	NOT_VR1: JNB 0E1H,NOT_VR2 ;SELECT VR2?
		286	ZSELECT_VR2
0146	800D	297	SJMP VR_SELECTED
		298	;
0148	30E20A	299	NOT_VR2: JNB 0E2H,VR_SELECTED ;SELECT VR3? IF NO THEN DO NOTHING
		300	ZSELECT_VR3
		310	;
		311	;
0155	E533	312	VR_SELECTED: MOV A,AMU_DW_EX ;SET UP SWEEP RATE
0157	B40602	313	CJNE A,#00H,LOAD_TIMER0 ;00 IS INVALID

```

000 GET      LIN.  SOURCE
015A 8408      314      SJMP   EXE_INC
                   315      ;
                   316      ;
015C 85318C    317      LOAD_TIMER0: MOV TH0,AMU_DW_EX      ;LOAD HI BYTE OF TIMER0
015F 75BA00    318      MOV     TL0,#00      ;LOW BYTE IS ALWAYS 00
0162 2164      319      AJMP   EXE_INC
                   320      ;
                   321      ;
0164 E574      322      EXE_INC: MOV     A,AMU_ST_EX      ;GET THE NEXT VALUE READY
0166 E572      323      ADD     A,AMU_INC_EX
0168 4011      324      JC      NXT_IS_LST      ;IF CFF THEN NEXT IS LAST
016A 853102    325      CJNE   A,AMU_E_EX,EX_NE_END
016D 800C      326      SJMP   NXT_IS_LST
016F 500A      327      EX_NE_END: JNC  NXT_IS_LST      ;END THEN NEXT IS LAST
0171 F530      328      MOV     AMU_ST_EX,A      ;SAVE NEXT AS VALID VALUE
0173 D2AB      329      SETB   ET1      ;ENABLE TIMER 1 ** TIMER 1 STARTS IF
                   330      ;
                   331      ;
                   332      ;      IF TR1 IS SET **** DON'T - F3 ****
0175 D2A9      333      SETB   ETO      ;ENABLE TIMER 0(SWEEP)
0177 D28C      334      SETB   TR0      ;START TIMER 0
0179 018E      335      AJMP   WAITINGCLR      ;THEN WAIT
017B 02F1      336      NXT_IS_LST: SETB E_OF_SW      ;TELL SWEEP THAT NEXT IS THE LAST
017D 853130    337      MOV     AMU_ST_EX,AMU_E_EX      ;LAST VALUE TO BE OUTPUT
0180 02AE      338      SETB   ET1      ;START TIMER 1 IF SENT 00
0182 D2A9      339      SETB   ETO      ;START TIMER0
0184 D28C      340      SETB   TR0
0186 018E      341      AJMP   WAITINGCLR
                   342      ;
                   343      ;
                   344      ;
                   345      ;
0188 842424    346      RATIO: CJNE   A,#2AH,TO_EXIT      ;WAS IT A RATIO COMMAND
018B 53023F    347      ANL     02,#3FH      ;STRIP OFF 2MSB OF DATA (R2)
018E BA0C02    348      CJNE   R2,#0CH,GT_OC      ;DATA=0CH?
0191 8002      349      SJMP   SET_RAT_CC      ;IF SO SET IT TO CC (MAX VAL ALLOWED)
                   350      ;
                   351      ;
0193 5005      352      GT_OC: JNC     EQ_33      ;< 0CH JUMP IF GREATER
0195 752ACC    353      SET_RAT_CC: MOV  T1_DW_H_I,#0CCH      ;0C MINIMUM VALUE ALLOWED
0198 8015      354      SJMP   TO_EXIT
                   355      ;
                   356      ;
019A BA3302    357      EQ_33: CJNE   R2,#3H,GT_33      ;=33H?
019D 8002      358      SJMP   SET_AT_3F      ;
                   359      ;
                   360      ;
019F 4005      361      GT_33: JC      IN_RAT      ;ACCEPT VALUE IF 33<V<CC
01A1 752A3F    362      SET_RAT_3F: MOV  T1_DW_H_I,#3FH      ;3F MAXIMUM VALUE ALLOWED
01A4 8009      363      SJMP   TO_EXIT

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LOC	OBJ	LINE	SOURCE	
		364	;	
		365	;	
01A6	EA	366	IN_RAT: MOV A,R2	;VALUE IS ACCEPTED BUT NEEDS MESSAGE
01A7	24C6	367	ADD A,#0CCH	;MAKE WORKING VALUE
		368	;	33<V+D0XCD
01A9	F52A	369	MOV T1_DW_H_I,A	;SAVE IT
01AB	EA	370	MOV A,R2	;GET ORIGINAL VALUE
01AC	FA	371	CPL A	;MESSAGE IT
01AD	F52B	372	MOV T1_DW_L_I,A	;SAVE IT
01AF	016E	373	TO_EXIT: AJMP WAITINGCLR	;AND WAIT
		374	;	
		375	;	
01B1	00	376	NOP	
01B2	00	377	NOP	
01B3	00	378	NOP	
01B4	00	379	NOP	
01B5	B2B1	380	TIMER_1_INT: CPL RAT_CLK	;TIMER JUST INTERRUPTS SO SWAP TIMES
01B7	B27B	381	CPL RAT_BIT_PTR	;POINT TO NEXT TIME INTERVAL
01B7	A62F	382	MOV R0,RAT_PTR	;MOVE POINTER TO R0
01BB	96BD	383	MOV TH1,@R0	; USE IT TO RELOAD TIMER
01BD	32	384	RETI	
01BE	00	385	NOP	
01BF	00	386	NOP	
01C0	00	387	NOP	
		388	;	
		389	;	
01C1	E0E0	390	SWEEP_INT: PUSH ACC	
01C3	20F056	391	JR ST_OF_SW,START_SWEEP	;START A NEW SWEEP?
01C4	20F1D5	392	JR E_OF_SW,LAST_OUTPUT	;LAST OUTPUT FOR CURRENT SWEEP?
01C9	8530B0	393	MOV BUS,AMU_ST_EX	;GET NEXT VALUE TO BE PUT OUT
01CC	E535	394	MOV A,VR_S_EX	;IS SWAP IN EFFECT?
01CE	20E30F	395	JR 0E3H,IS_SWAP	
		396	XTO65LE(AMU)	
01D5	E530	400	INC_AMU: MOV A,AMU_ST_EX	;GET VALUE JUST PUT OUT
01D7	7532	401	ADD A,AMU_INC_EX	;ADD THE INC VALUE
01D9	401C	402	JC SET_LAST	;IF >FF THEN NEXT WILL BE END
01DB	25310B	403	CJNE A,AMU_E_EX,NE_LAST	;= END VALUE?
01DE	8017	404	SJMP SET_LAST	
		405	IS_SWAP: XTO66L(IVR)	
01E4	80EF	409	SJMP INC_AMU	
01E6	500F	410	NE_LAST: JNC SET_LAST	;IF > END VAL THEN NEXT WILL BE LAST
01E8	F530	411	MOV AMU_ST_EX,A	
01EA	8533B0	412	SWEEP_EXIT: MOV TH0,AMU_DW_EX	;RESET SWEEP TIME
01ED	75BA00	413	MOV TLO,#00H	
01F0	D2A9	414	SETB ETO	
01F2	D2BC	415	SETB TRO	
01F4	D0E0	416	POP ACC	
01F6	32	417	RETI;	OUTPUT IS KNOWN (AMU_S_EX)
		418	;	
		419	;	

LOC	OBJ	LINE	SOURCE	
01F7 02F1		400	SET_LAST: SETB E_OF_SW	;SET END OF SWEEP FLAG
01F9 853130		401	MOV AMU_ST_EX,AMU_E_EX	;SAVE END VALUE
01FC 51ED		402	SJMP SWEEP_EXIT	;AND EXIT
		403	:	
		404	:	
01FE 02F1		405	LAST_LOOK: CLR E_OF_SW	;NEXT IS NOT LAST
0200 02F0		406	SETB ST_OF_SW	;NEXT IS BEGINING
0202 853180		407	MOV SUB,AMU_E_EX	;GET LAST VALUE
0205 8535		408	MOV H_VR,S_EX	;CHECK FOR SWAP
0207 02EDF		409	JB DECH,LAST_SWAP	
		410	XTOGGLE(AMU)	
020E 853430		414	MOV AMU_ST_EX,AMU_ST_0	;NEXT IS START
0211 8007		415	SJMP SWEEP_EXIT	;AND LEAVE
		416	:	
		417	:	
		418	LAST_SWAP: XTOGGLE(VR)	
0217 853430		442	MOV AMU_ST_EX,AMU_ST_0	;NEXT IS START
021A 51DE		443	SJMP SWEEP_EXIT	
		444	:	
		445	:	
021C 02F0		446	START_SWEEP: CLR ST_OF_SW	;RESET FLAG
021E 02F2		447	CLR FIRST_SWEEP	;HAS COMPLETED AT LEAST SW FROM EX
0220 853080		448	MOV SUB,AMU_ST_EX	
0223 8535		449	MOV A,VR,S_EX	;IS SWAP IN EFFECT?
0225 20E306		450	JB DECH,START_SWAP	
		451	XTOGGLE(AMU)	
022E 8004		455	SJMP ISO_IN	;LATCH IN ISO METER ?
		456	:	
		457	:	
		458	START_SWAP: XTOGGLE(VR)	
0232 30E1A0		462	ISO_IN: JNB GE1H,INC_AMU	;IF NOT VR2 THEN JUMP
0235 02B5		463	CLR VR2	
0237 02B5		464	SETB VR2	
0239 02B5		465	SETB VR2	
023B 02B5		466	CLR VR2	
023D 8096		467	SJMP INC_AMU	;GET THE NEXT VALUE THEN EXIT
		468	END	

400 SYMBOL TABLE LISTING

NAME	TYPE	VALUE	ATTRIBUTE AND REFERENCES
ADD	D ADDR	00E0H A	190 416
AMU_IN_D	NUMB	00F4H A	194 136
AMU_IN_EX	D ADDR	0073H A	554 312 317 412
AMU_IN_I	D ADDR	0023H A	554 136
AMU_IN_O	NUMB	0074H A	274 134
AMU_IN_EY	D ADDR	0031H A	524 325 337 403 401 427
AMU_IN_I1	D ADDR	0021H A	514 134
AMU_INO_D	NUMB	0001H A	284 136
AMU_INO_EX	D ADDR	0032H A	544 323 401
AMU_INO_I	D ADDR	0022H A	534 136
AMU_INO_O	NUMB	0019H A	264 133
AMU_INO_EX	D ADDR	0030H A	494 249 322 328 337 393 400 411 421 434 442 448
AMU_INO_I1	D ADDR	0020H A	484 133
AMU_INO_O	D ADDR	0034H A	504 434 442
AMU_INO_O	B ADDR	00A0H A	794 253 254 271 272 397 398 431 432 452 453
ADD_OF	D ADDR	0070H A	109 1194
ADD	D ADDR	0080H A	204 249 256 269 293 427 148
COMMAND	D ADDR	00A0H A	214 184
DATA_BUS	D ADDR	0090H A	224 183
DEF_L	B ADDR	00B0H.7 A	784 166 208
DEF_SW	B ADDR	00F0H.1 A	854 210 336 392 420 425
END_EXIT	C ADDR	00B0H A	189 1944
END	C ADDR	00A5H A	1894 195
END_3	C ADDR	019AH A	352 3574
END	B ADDR	00A6H.1 A	209 215 333 339 414
END	B ADDR	00A6H.0 A	216 329 338
END_EXD	C ADDR	016FH A	325 3274
END_FROM_RESET	C ADDR	00E4H A	170 2094
END_INO	D ADDR	0164H A	314 319 3224
END_INO	B ADDR	00F0H.3 A	894
END	C ADDR	00C2H A	206 2094
END_SWEEP	B ADDR	00F0H.2 A	864 18 212 447
END	C ADDR	019FH A	357 36 4
END	C ADDR	019FH A	344 35 4
END	C ADDR	00A6H A	160
END	B ADDR	00B8H.3 A	176 17 194
END	C ADDR	01A6H A	361 36 4
END_AMU	C ADDR	01D5H A	4004 4 4 462 457
END	C ADDR	0090H A	177 18 4
END	D ADDR	00B9H A	164
END_SWAP	C ADDR	01E0H A	395 40 4
END_IN	C ADDR	0232H A	455 46 4
END_OUTPUT	C ADDR	01FEH A	392 40 4
END_SWAP	D ADDR	0213H A	424 43 4
END_TIMER	C ADDR	015CH A	313 31 4
END_LAST	C ADDR	01E6H A	403 41 4



NAME	TYPE	VALUE	ATTRIBUTES AND REFERENCES
NOT_ECI	D ADDR	00B4H A	188 201#
NOT_EYS	D ADDR	00C0H A	205 207#
NOT_VR1	D ADDR	0137H A	261 295#
NOT_VR2	D ADDR	0148H A	285 299#
NOT_IS_LST	D ADDR	017BH A	324 326 327 328#
FI	D ADDR	0180H A	21
FI	D ADDR	0190H A	22
FI	D ADDR	01A0H A	23
RAT_BIT_PTR	B ADDR	002FH.0 A	51# 381
RAT_DLF	B ADDR	00B0H.1 A	33# 235 240 247 380
RAT_NOT_CC	D ADDR	00F6H A	274 279#
RAT_NOT_F3	D ADDR	00FFH A	239 244#
RAT_PTR	D ADDR	012FH A	15# 141 246 352
RATIC	D ADDR	015BH A	207 346#
READ_LINE	B ADDR	00A7H.3 A	51# 149 156 196 204
RESET_INH	B ADDR	00B0H.2 A	98# 179 180 191 192
RESET	D ADDR	00C0H A	108
SET_LAST	D ADDR	01F7H A	402 404 410 423#
SET_PAT_DF	D ADDR	01A1H A	358 362#
SET_RAT_CC	D ADDR	01F5H A	349 353#
SET_TO_ZERO	D ADDR	0035H A	123# 125
SP	D ADDR	0081H A	159
ST_OF_SW	B ADDR	00F0H.0 A	34# 211 291 426 446
START_SWAP	D ADDR	002EH A	450 458#
START_SWEEP	D ADDR	0210H A	391 446#
STROBE	B ADDR	00B0H.3 A	87#
STRT_TIMER	D ADDR	010CH A	238 241 249#
SV1	D ADDR	012FH A	262 274#
SWEEP_EXIT	D ADDR	015AH A	412# 422 475 443
SWEEP_INT	D ADDR	01C1H A	111 390#
TI_DW_H_D	NUMB	00CFH A	32# 139
TI_DW_H_EX	D ADDR	003AH A	70# 167 233 245
TI_DW_H_L	D ADDR	002AH A	68# 139 353 362 369
TI_DW_L_D	NUMB	00F0H A	33# 146
TI_DW_L_EX	D ADDR	003BH A	71# 166 244
TI_DW_L_L	D ADDR	002BH A	69# 140 372
TCON	D ADDR	008BH A	161
TH0	D ADDR	008CH A	317 412
TH1	D ADDR	008DH A	167 245 373
TIMER_1_INT	D ADDR	01B5H A	113 380#
TIMER0	D ADDR	000EH A	110
TIMER1	D ADDR	001EH A	112
TLO	D ADDR	008EH A	318 413
TL1	D ADDR	008FH A	166 244
TMOD	D ADDR	0089H A	162
TO_EXIT	D ADDR	01AFH A	346 354 363 373#
TR0	B ADDR	0089H.4 A	212 334 340 415
TR1	B ADDR	0089H.6 A	214 248
VR_AMU_SWAP	D ADDR	0124H A	251 265#
VR_S_D	NUMB	0004H A	30# 137

NAME	TYPE	VALUE	ATTRIBUTES AND REFERENCES
BASELBY	B ADDR	0035H A	60# 250 394 428 449
BASEL	D ADDR	0025H A	59# 137
BASEL ECTROL	D ADDR	0135H A	282 297 299 312#
BASEL	NAME	0000H A	31# 138
BASEL EX	D ADDR	0036H A	62# 255 269
BASEL	D ADDR	0026H A	61# 138
BASEL	B ADDR	0040H.1 A	80# 258 259 266 277 406 407 439 440 459 460
BASEL	B ADDR	0050H.4 A	75# 286 290 305 316 307
BASEL	B ADDR	0060H.5 A	76# 278 292 293 314 295 304 463 464 465 466
BASEL	B ADDR	0060H.6 A	77# 279 291 306
BASEL	D ADDR	0090H A	177# 182
BASEL	D ADDR	0093H A	178#
BASEL	D ADDR	008EH A	176# 197 335 341 373

REGISTER BANK(S) USED: 0

ASSEMBLY COMPLETE. NO ERRORS FOUND

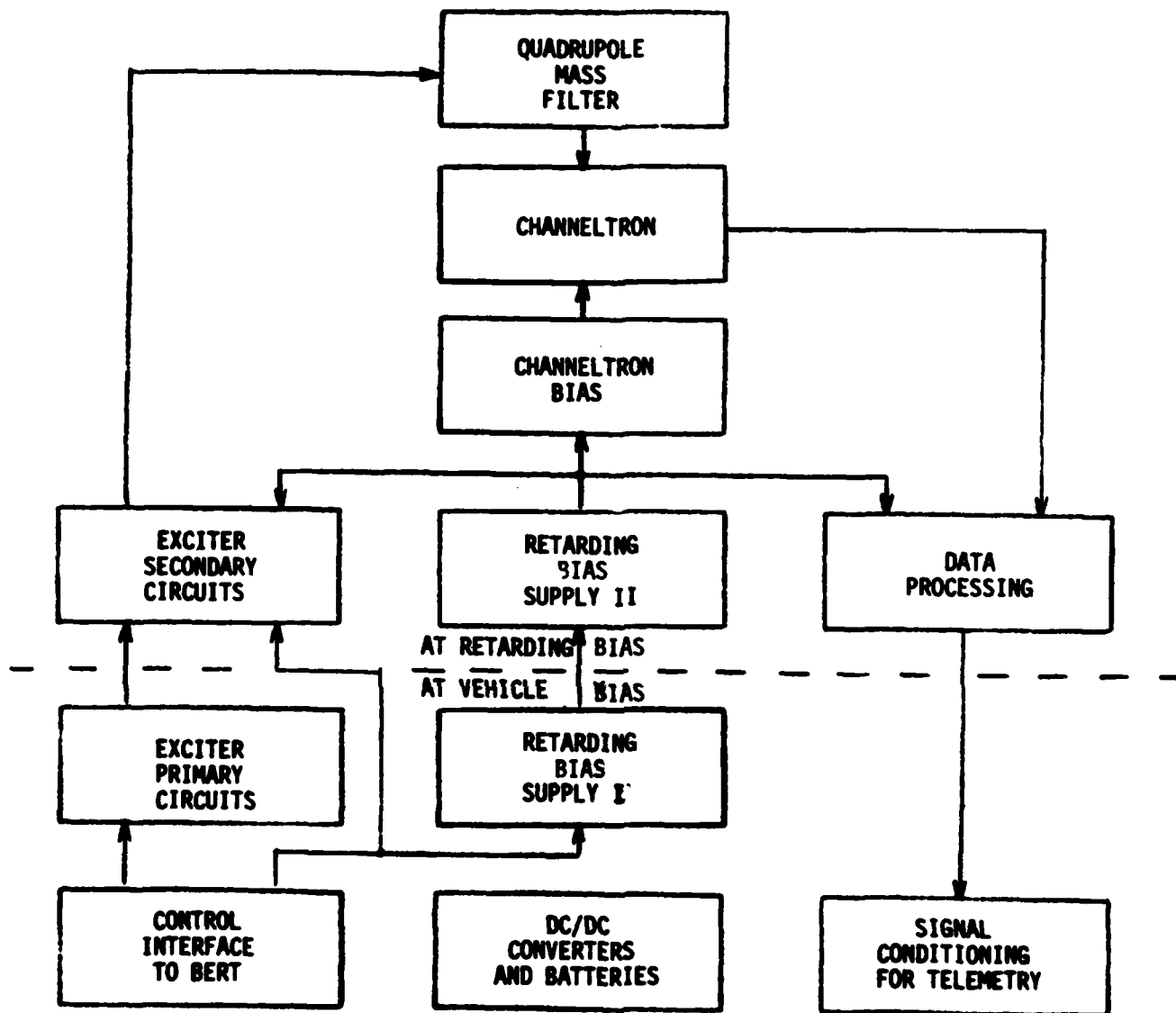
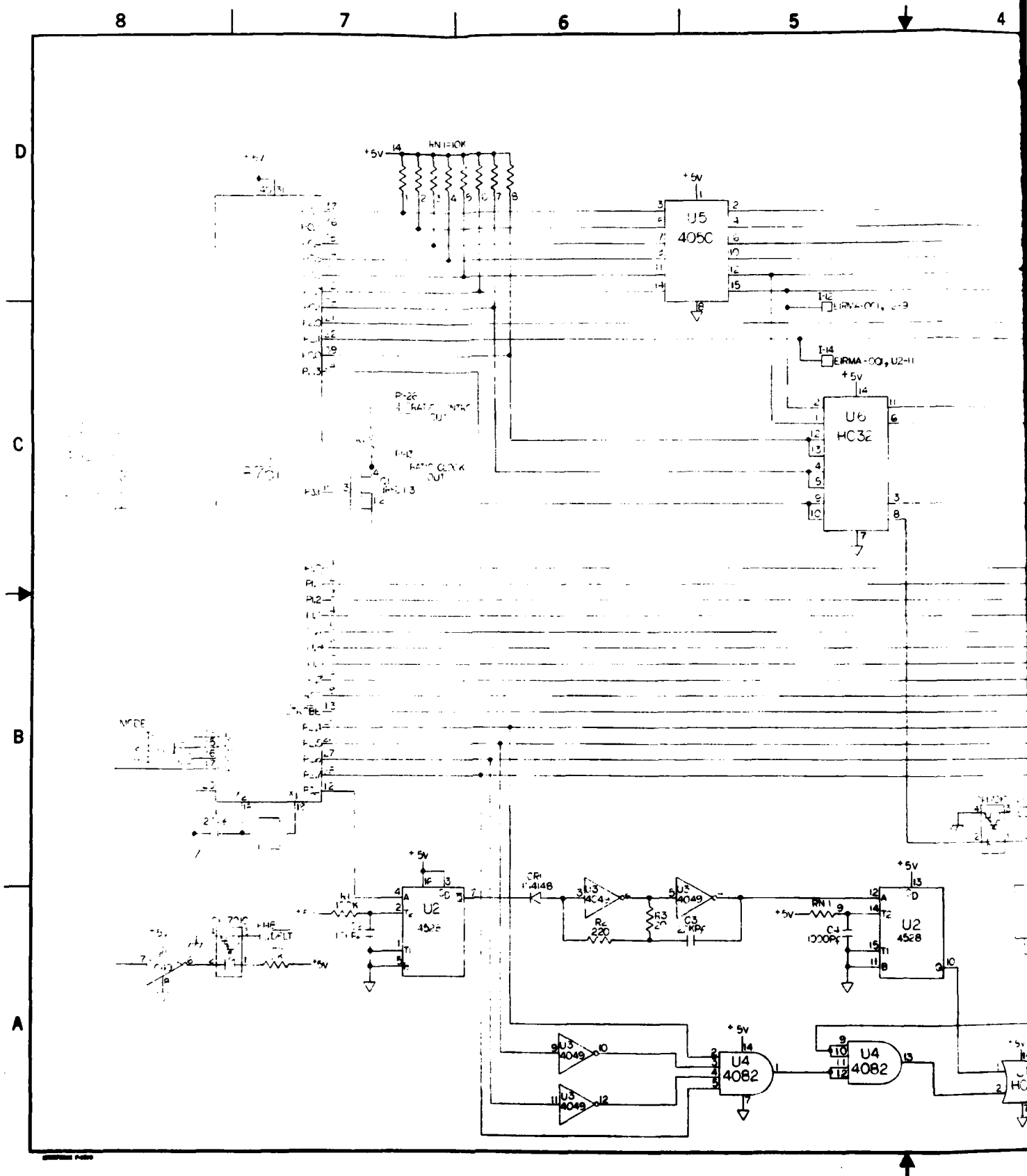


FIGURE 1. BLOCK DIAGRAM OF EIRMA



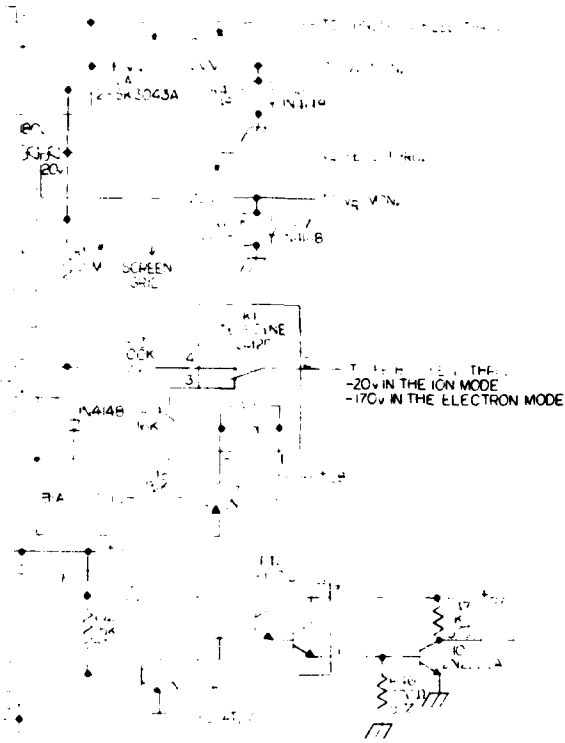






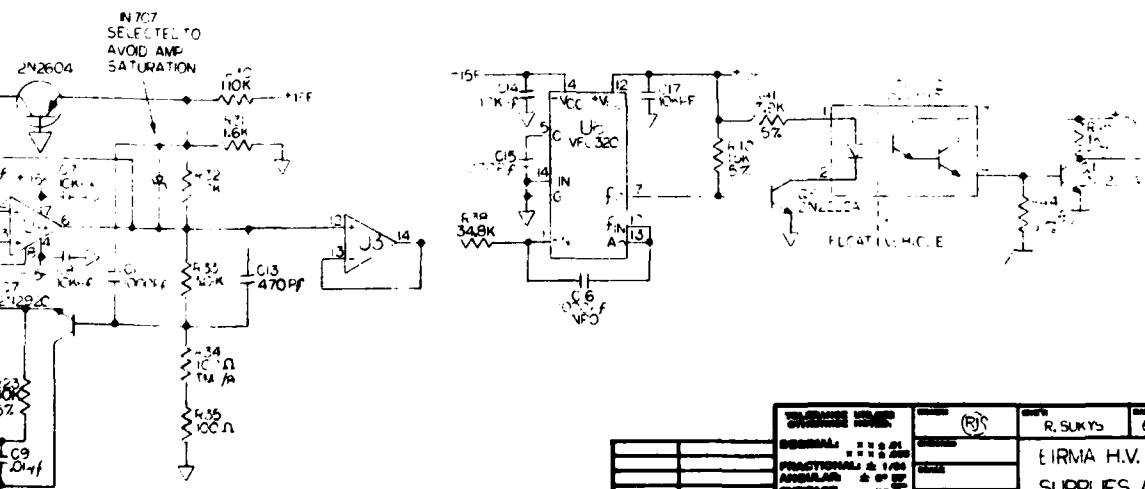






NOTE: IN ALL CASES THE  
 -20V IN THE ION MODE  
 -170V IN THE ELECTRON MODE

/// DENOTES INSTRUMENT GROUND



DESIGNER: R. SUKYS DATE: 6/20/94		NORTHWESTERN UNIVERSITY LINCOLN COLLEGE COLLEGE OF ENGINEERING BOSTON, MASS. 02115
EIRMA H.V. SUPPLIES AND DATA CIRCUITS FIGURE 4		
APPLICATION:		EIRMA-004



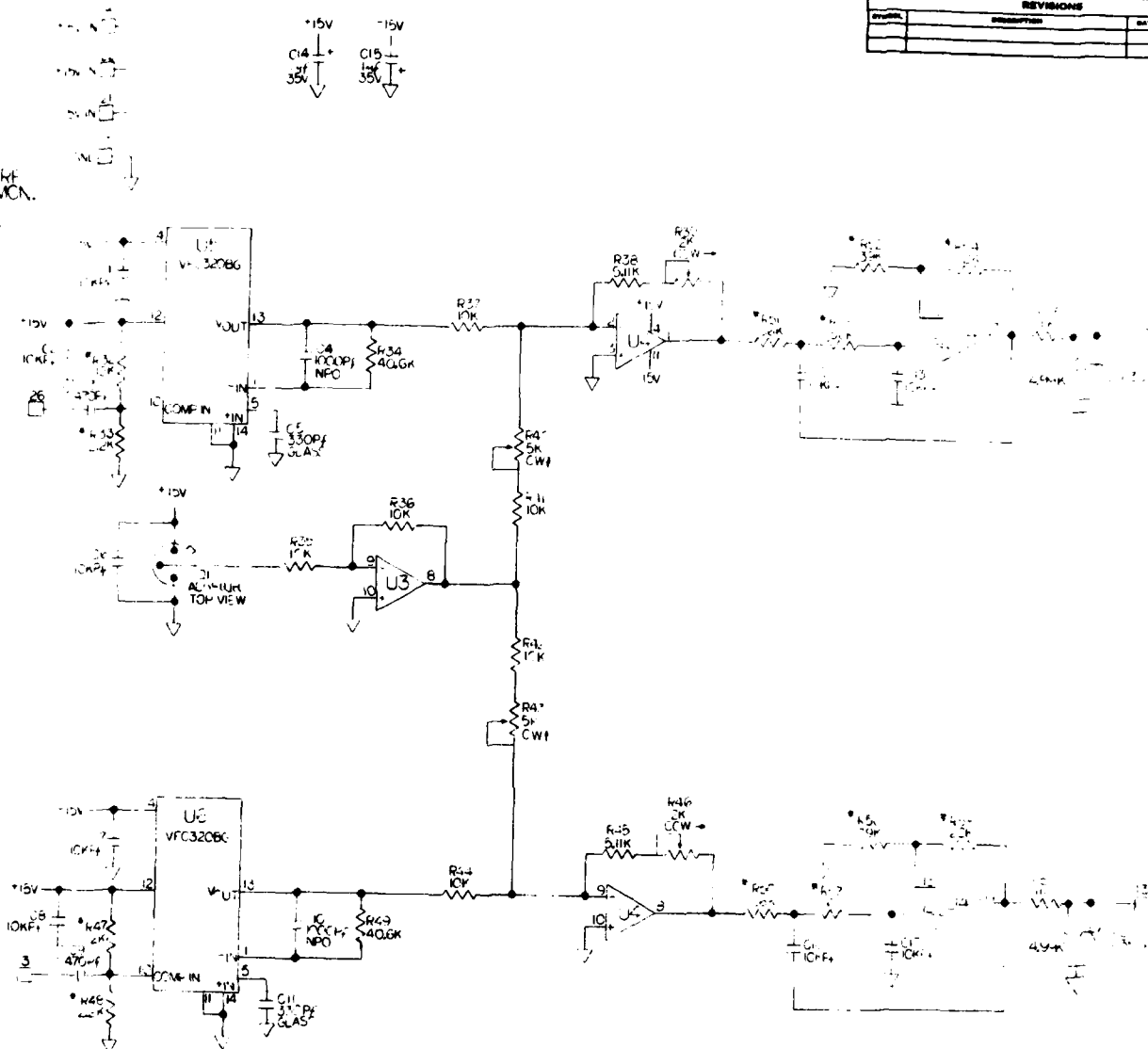
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REVISIONS			
NO.	DESCRIPTION	DATE	APPROVAL



NOTES: 1. U1-U4 ARE HARRIS 4002.  
2. RESISTORS DENOTED BY \* ARE 1/4W, 5% TOLERANCE.

DESIGNER: R. J. LUKYS		DATE: 5/1/70	
PROJECT: CIRMA SPECT. - FLUX SIGNAL COND. CIRCUITS & CIRMA MONITORS		FIGURE 5	
APPROVED: [Signature]		NORTHEASTERN UNIVERSITY LINCOLN COLLEGE COLLEGE OF ENGINEERING BOSTON, MASS. 02115	
APPLICATION: [Blank]		EIRMA-003	

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## VI. PERSONNEL

A list of the engineers who contributed to the work reported is given below:

J. Spencer Rochefort, Professor of Electrical and Computer Engineering and Principal Investigator.

Raimundas Sukys, Senior Research Associate, Engineer.

## VII. RELATED CONTRACTS AND PUBLICATIONS

F19628-74-C-0042	1 September 1973 through October 1976
F19628-76-C-0256	1 August 1976 through 31 October 1978
F19628-78-C-0218	15 September 1978 through September 1981
F19628-81-C-0162	15 September 1981 through present.

Raimundas Sukys, Steven Goldberg, "Control Circuits for Rocket Payload Neutralization Experiment and Other Topics", Scientific Report No. 1 for Contract F19628-74-C-0042, October 1974, AFGRL-TR-74-0580, ADA008039.

R. Sukys, J. Spencer Rochefort, S. Goldberg, "Bias and Signal Processing Circuits for a Mass Spectrometer in the Project EXCEDE: SWIR Experiment", Scientific Report No. 2 for Contract F19628-74-C-0042, October 1975, AFGL-TR-76-0060, ADA026514.

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Gerousis, V.S., "A Programmable Control Unit for a Balloon-Borne Mass Spectrometer Based on Intel 8085A Microprocessor", Scientific Report No. 1, Contract AF19628-78-C-0218, September 1979, AFGL-TR-79-0225, ADA106398.

Palasek, T., "An RF Oscillator for Rocket-Borne and Balloon-Borne Mass Spectrometers", Scientific Report No. 2, Contract AF19628-78-C-0218, September 1979, AFGL-TR-79-0226, ADA078797.

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J. Spencer Rochefort, Raimundas Sukys, "Control Electronics for Airborne Quadrupole Ion Mass Spectrometer", Final Report for Contract F19628-78-C-0218, October 1981, AFGL-TR-82-0056, ADA115399.

VII. RELATED CONTRACTS AND PUBLICATIONS (cont.)

Sukys, R. and Rochefort, J.S. "GSE for Balloon Borne I.M.S.: Decomm-  
tator and D/A Units", Scientific Report No. 1 for Contract F19628-81-C-  
0162, October 1982, AFGL-TR-83-0095, ADA131845.

Sukys, R. and Rochefort, J.S. "Downrigger Instrumentation to Record  
Thermosonde Data", Scientific Report No. 2 for Contract F19628-81-C-  
0162, October 1983, AFGL-TR-85-0085, ADA161748

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